

An Experimental Study on the Flexural Strength of Fiber Reinforced Concrete Structures

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Abstract : In this thesis, fracture tests were carried out in order to investigate the flexural strength behavior of FRC(fiber reinforced concrete) structures. FRC beams were used in the tests, the initial crack load and the ultimate load of the beams were observed under the static loading. According to the results, the ultimate loads increase with the fiber content, and these tendency is clear in the specimens with large fiber aspect ratio. From the results of the regression analysis, practical formulae for predicting the flexural strength of FRC were suggested.

Key words : fracture test, fiber reinforced concrete, flexural strength, average spacing, practical formulae

1. Introduction

From the results of previous studies, the mechanism of the FRC beams under static loading has been well known, but recently it has become necessary to know the initial crack load, the ultimate load and the flexural strength of the FRC beams.

Romualdi and Batson [1, 2] studied the mechanism of FRC firstly. Romualdi and Mandel [3] showed that the tensile strength of concrete is dependent upon the spacing of fibers. Chai [4] studied that when the fiber content is 2.0% the estimated tensile strength was 0.15 times of the average compressive strength.

On this basis, in this study, the initial crack load and the ultimate load of FRC beams under static loading has been investigated. In this work, the relationship between the fiber content and the ultimate load, the relationship between the average spacing of random fiber and the initial crack load, and the relationship between the fiber content multiplication the aspect ratio and the flexural strength have been studied.

2. Test Program

The fibers with diameter of 0.9 mm were used to reinforce the concrete beams. Density, elastic modulus and tensile strength of the fiber are 78.5 KN/m³, 200 GPa,

Table 1. Mix proportion of concrete

W(N/m ³)	C(N/m ³)	S(N/m ³)	G(N/m ³)
1814	4272	7375	9179

and 1275 MPa, respectively.

The portland cement was used and the maximum size of coarse aggregate is 19 mm. The used mix proportion is shown in Table 1. Where W is water content, C is cement content, S is fine aggregate content, and G is coarse aggregate content, respectively.

Beam specimen of 100 mm×100 mm×600 mm are used. The specimen series are classified according to the fiber contents varying 0.0%, 0.5%, 1.0%, 1.5%, and to the fiber aspect ratios 60, 80, 100.

The three point loading system is used in the fracture tests. In these tests, the initial crack load and the ultimate load were detected.

3. Results of Fracture Test

3.1 Relationship between the fiber content and the ultimate load

As shown in Fig. 1, the ultimate loads increase with the fiber content, and these tendency is clear in the specimens with large fiber aspect ratio. By taking average value of the ultimate loads, it could be said that the ultimate loads of the specimens with the fiber aspect ratio

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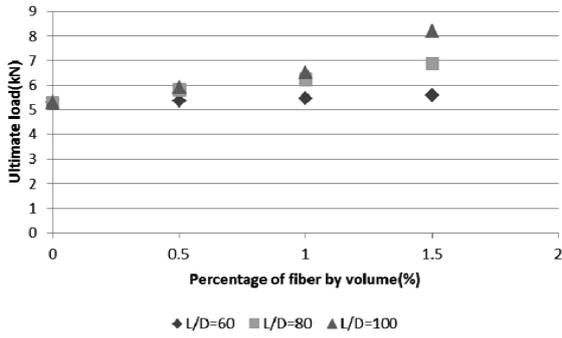


Fig. 1. Relationship between the fiber content and the ultimate load.

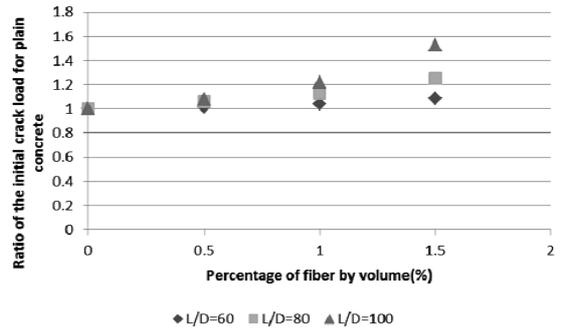


Fig. 3. Relationship between the fiber content and the ratio of the initial crack load for plain concrete.

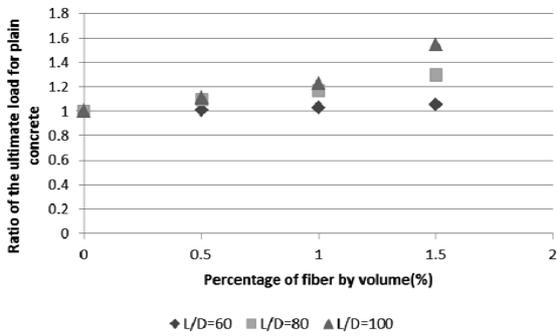


Fig. 2. Relationship between the fiber content and the ratio of the ultimate load for plain concrete.

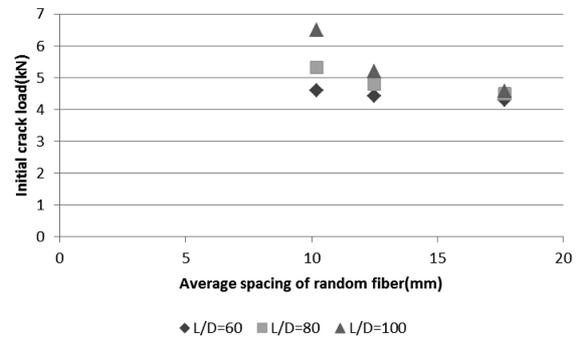


Fig. 4. Relationship between the average spacing of random fiber and the initial crack load.

of 100 are increased as 1.25 times, as compared with that of the specimens with the fiber aspect ratio of 60.

In addition, from Fig. 2, it can be concluded that the effects on the ultimate load can hardly be expected in concrete with fiber content below 0.5%. But when the fiber content is 1.5%, the ultimate load of FRC specimens is increased 1.3 times of that of the plain concrete specimen. We can also find that even specimens have the same fiber content, the larger the fiber aspect ratio is, the larger the ultimate load increases.

3.2 Relationship between the average spacing of random fibers and the initial crack load

As shown in Fig. 3, the initial crack loads increase with the fiber content like the ultimate load, and these tendency is clear in the specimens with large fiber aspect ratio.

The relationship between the number of fibers per unit volume of FRC, N , and the number of fibers crossing over a unit cross section, n , are as follows:

$$N = \frac{V_f}{25\pi D^2 L} = \frac{n}{\beta L} \quad (1)$$

Where, V_f is the fiber content, D is the diameter of a fiber, L is the length of a fiber, and β is the effectiveness factor of random fiber.

For $\beta = 0.405$ according to Romualdi's theory [2], the average spacing of random fibers, s , can be written as follows:

$$s^2 = \frac{1}{n} \quad (2)$$

$$s = \sqrt{\frac{1}{n}} = \sqrt{\frac{25\pi D^2}{V_f \beta}} = 13.9 \frac{D}{\sqrt{V_f}} \quad (3)$$

Applying the average spacing of random fibers by Romualdi's theory, we can compare the initial crack loads with the average spacing of random fibers as shown in Fig. 4. This figure indicates that, if the average spacing of random fibers is less than about 15 mm, the initial crack load of FRC is increased rapidly.

3.3 Flexural strength

The flexural strength is observed in order to find the crack-growth-limiting capacity of FRC for the changes of the fiber content and the fiber aspect ratio.

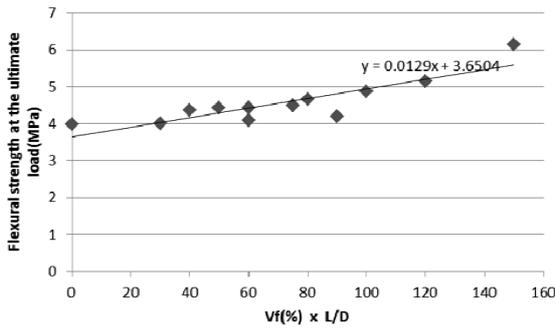


Fig. 5. Relationship between the fiber content multiplication the aspect ratio and the flexural strength.

In this thesis, on the basis of the above equation, the flexural strength is presented as follows.

$$f_{cf} = A + B \cdot V_f \cdot \left(\frac{L}{D}\right) \quad (4)$$

Where, f_{cf} is the flexural strength of FRC at the ultimate load, V_f is the fiber content, L/D is the fiber aspect ratio, and A and B are the experimental constants.

The results of the regression are shown in Fig. 5. From these results, the flexural strength of FRC could be predicted as follows:

$$f_{cf} = 3.65 + 0.103 \times V_f \cdot \left(\frac{L}{D}\right) \quad (5)$$

4. Conclusions

1. The ultimate loads increase with the fiber content,

and these tendency is clear in the specimens with large fiber aspect ratio. The ultimate load of FRC could be increased 1.3 times of that of plain concrete by using the fiber content of 1.5%.

2. Although the same fiber content is used, the ultimate load of FRC could be increased more using larger the fiber aspect ratio. The ultimate loads of the specimens with the fiber aspect ratio of 100 are increased as 1.25 times, as compared with that of the specimens with the fiber aspect ratio of 60.

3. The initial crack load of FRC is increased largely when the average spacing of random fibers is less than about 15 mm.

4. Practical formulae for predicting the flexural strength of FRC are suggested.

References

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