

NFL-ROO 에 기준한 SMC 의 안정도 증명 : Part 6

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Stability Proof of NFL-ROO-based SMC : Part 6

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[Abstract] This paper presents the stability proof of a nonlinear feedback linearization-reduced order observer-based sliding mode controller (NFL-ROO-based SMC). The closed-loop stability is proved by a Lyapunov function candidate using an addition form of the sliding surface vector and the estimation error.

Keywords : nonlinear feedback linearization-reduced order observer-based sliding mode controller, Lyapunov function, stability proof

1. Introduction

In this paper, a nonlinear feedback linearization-reduced order observer-based sliding mode controller (NFL-ROO-based SMC) to design the simpler observer-based controller, and to solve the problem associated with the unmeasurable state variables in the conventional SMC is developed [1-18]. The proposed NFL-ROO-based SMC is obtained by the estimated state variable based on observer state in designing a sliding surface gain to ensure the stability by Lyapunov's method. The closed-loop stability is proved by a Lyapunov function candidate using an addition form of the sliding surface vector and the estimation error.

2. NFL-ROO-based SMC

The state equation for full-state feedback and the output equation based on nonlinear feedback linearization (NFL) can be expressed as [19]

$$z(t) = T(x(t)) \quad (1)$$

$$\dot{z}(t) = Az(t) + Bu(t) \quad (2)$$

$$y(t) = Cz(t) \quad (3)$$

The transformation matrix is introduced by

$$q(t) = Tz(t) \quad (4)$$

$$\begin{bmatrix} y(t) \\ q(t) \end{bmatrix} = \begin{bmatrix} C \\ T \end{bmatrix} z(t) \quad (5)$$

$$z(t) = \begin{bmatrix} C \\ T \end{bmatrix}^{-1} \begin{bmatrix} y(t) \\ q(t) \end{bmatrix} = [P \quad M] \begin{bmatrix} y(t) \\ q(t) \end{bmatrix} = Py(t) + Mq(t) \quad (6)$$

The estimate \hat{z} of z is generated as

$$\dot{\hat{z}}(t) = Py(t) + M\dot{q}(t) \quad (7)$$

A new realization for the system is expressed as

$$E\dot{z}(t) = EAz(t) + EBU(t) \quad (8)$$

Substituting for z and E , we get

$$\begin{aligned} E\dot{z}(t) &= \begin{bmatrix} C \\ T \end{bmatrix} \dot{z}(t) = \begin{bmatrix} \dot{y}(t) \\ \dot{q}(t) \end{bmatrix} = \begin{bmatrix} C \\ T \end{bmatrix} Az(t) + \begin{bmatrix} C \\ T \end{bmatrix} Bu(t) \\ &= \begin{bmatrix} C \\ T \end{bmatrix} A [P \quad M] \begin{bmatrix} y(t) \\ q(t) \end{bmatrix} + \begin{bmatrix} C \\ T \end{bmatrix} Bu(t) \end{aligned} \quad (9)$$

Therefore, we get

$$\begin{bmatrix} \dot{y}(t) \\ \dot{q}(t) \end{bmatrix} = \begin{bmatrix} CAP & CAM \\ TAP & TAM \end{bmatrix} \begin{bmatrix} y(t) \\ q(t) \end{bmatrix} + \begin{bmatrix} CB \\ TB \end{bmatrix} u(t) \quad (10)$$

$$:= \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} y(t) \\ q(t) \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} u(t) \quad (11)$$

$$\dot{y}(t) = A_{11}y(t) + A_{12}q(t) + B_1u(t) \quad (12)$$

$$\dot{q}(t) = A_{22}q(t) + A_{21}y(t) + B_2u(t) \quad (13)$$

The estimator equation for q is

$$\dot{\hat{q}}(t) = A_{22}\hat{q}(t) + A_{21}y(t) + B_2u(t) + L(y(t) - C\hat{z}(t)) \quad (14)$$

Let $CP = I$ and $CM = 0$

$$\begin{aligned} y(t) - C\hat{z} &= y(t) - C(Py(t) + M\hat{q}) \\ &= y(t) - CPy(t) - CM\hat{q} = y(t) - y(t) - 0 = 0 \end{aligned} \quad (15)$$

The reduced-order observer is represented by

$$\begin{aligned} \dot{\hat{q}}(t) &= A_{22}\hat{q}(t) + A_{21}y(t) + B_2u(t) \\ &\quad + L(y(t) - A_{21}y(t) - B_2u(t) - A_{22}\hat{q}(t)) \end{aligned} \quad (16)$$

Define w and \dot{w} , we get

$$w(t) := \hat{q}(t) - Ly(t) \quad (17)$$

$$\dot{w}(t) := \dot{\hat{q}}(t) - L\dot{y}(t) \quad (18)$$

The final form of the reduced-order observer is

$$\dot{w}(t) = (A_{22} - LA_{12})w(t) + [(A_{22} - LA_{12})L + A_{21} - LA_{11}]y(t) + (B_2 - LB_1)u(t) \quad (19)$$

$$\hat{z}(t) = Mw(t) + (P + ML)y(t) \quad (20)$$

$$\dot{\hat{z}}(t) = M\dot{w}(t) + (P + ML)\dot{y}(t) \quad (21)$$

The equations (19) and (20) are simplified as [1]

$$\dot{w}(t) = Fw(t) + Gy(t) + Hu(t) \quad (22)$$

$$\hat{z}(t) = Mw(t) + Ny(t) \quad (23)$$

where, $F := (A_{22} - LA_{12})$ (24)

$$G := [(A_{22} - LA_{12})L + A_{21} - LA_{11}] \quad (25)$$

$$H := (B_2 - LB_1) \quad (26)$$

$$N := (P + ML) \quad (27)$$

The sliding surface vector and the differential sliding surface vector based on NFL are

$$\hat{z} = T^{-1}\hat{q} \quad (28)$$

$$\dot{\sigma}(\hat{z}(t)) = G_{ss}^T \dot{\hat{z}}(t) \quad (29)$$

The Lyapunov's function is

$$V(\hat{z}(t)) = \sigma^T(\hat{z}(t)) / 2 \quad (30)$$

The time derivative of $V(\hat{z}(t))$ is expressed as

$$\dot{V}(\hat{z}(t)) = \sigma(\hat{z}(t))\dot{\sigma}(\hat{z}(t)) \quad (31)$$

$$\begin{aligned} &= G_{ss}^T \dot{\hat{z}}(t) G_{ss}^T \hat{z}(t) = G_{ss}^T \dot{\hat{z}}(t) G_{ss}^T [M\dot{w}(t) + (P + ML)\dot{y}(t)] \\ &= G_{ss}^T \dot{\hat{z}}(t) G_{ss}^T [M((A_{22} - LA_{12})L + A_{21} - LA_{11})y(t) \\ &\quad + ((A_{22} - LA_{12})L + A_{21} - LA_{11})y(t) \\ &\quad + (B_2 - LB_1)u_{ROO-SMC}(t) + (P + ML) \\ &\quad (A_{11}y(t) + A_{12}q(t) + B_1u_{ROO-SMC}(t))] \\ &= G_{ss}^T \dot{\hat{z}}(t) [G_{ss}^T M(A_{22} - LA_{12})w(t) \\ &\quad + (G_{ss}^T M(A_{22} - LA_{12})L + G_{ss}^T MA_{21} \\ &\quad - G_{ss}^T MLA_{11} + G_{ss}^T (P + ML)A_{11})y(t) \\ &\quad + (P + ML)A_{12}q(t) + (MB_2 + PB_1)u_{ROO-SMC}(t)] \leq 0 \quad (32) \end{aligned}$$

The control inputs with switching function are

$$\begin{aligned} u_{ROO-SMC}(t) \geq & -[G_{ss}^T (MB_2 + PB_1)]^{-1} [G_{ss}^T (MA_{22} - MLA_{12})w(t) \\ & + G_{ss}^T (M(A_{22} - LA_{12})L + MA_{21} + PA_{11})y(t) \\ & + G_{ss}^T (P + ML)A_{12}q(t)] \quad \text{for } G_{ss}^T \dot{\hat{z}}(t) > 0 \quad (33) \end{aligned}$$

$$\begin{aligned} u_{ROO-SMC}(t) \leq & -[G_{ss}^T (MB_2 + PB_1)]^{-1} [G_{ss}^T (MA_{22} - MLA_{12})w(t) \\ & + G_{ss}^T (M(A_{22} - LA_{12})L + MA_{21} + PA_{11})y(t) \\ & + G_{ss}^T (P + ML)A_{12}q(t)] \quad \text{for } G_{ss}^T \dot{\hat{z}}(t) < 0 \quad (34) \end{aligned}$$

The estimated control input with sign function is

$$\hat{u}_{ROO-SMC}^{ign}(t) = -[G_{ss}^T (MB_2 + PB_1)]^{-1} [G_{ss}^T (MA_{22} - MLA_{12})w(t)$$

$$\begin{aligned} & + G_{ss}^T (M(A_{22} - LA_{12})L + MA_{21} + PA_{11})y(t) \\ & + G_{ss}^T (P + ML)A_{12}q(t)] \text{ sign}(\sigma(\hat{z}(t))) \quad (35) \end{aligned}$$

The equation (35) is simplified as follows

$$\hat{u}_{ROO-SMC}^{ign}(t) = -[RGK_1 w(t) + RGK_2 y(t) + RGK_3 q(t)] \text{ sign}(\sigma(\hat{z}(t))) \quad (36)$$

where,

$$RGK_1 := [G_{ss}^T (MB_2 + PB_1)]^{-1} G_{ss}^T M(A_{22} - LA_{12}) \quad (37)$$

$$RGK_2 := [G_{ss}^T (MB_2 + PB_1)]^{-1} \quad (38)$$

$$G_{ss}^T (M(A_{22} - LA_{12})L + MA_{21} + PA_{11}) \quad (38)$$

$$RGK_3 := [G_{ss}^T (MB_2 + PB_1)]^{-1} G_{ss}^T (P + ML)A_{12} \quad (39)$$

Theorem 1: Consider the full state equation based on NFL for the regulation problem and the reduced order observer problem based on NFL

$$\dot{z} = Az + B\hat{u}_{ROO-SMC}^{ign} \quad \text{and} \quad y = Cz$$

$$\dot{\hat{z}} = M\dot{w} + (P + ML)\dot{y}$$

$$\dot{w} = (A_{22} - LA_{12})w + [(A_{22} - LA_{12})L + A_{21} - LA_{11}]y$$

$$+ (B_2 - LB_1)\hat{u}_{ROO-SMC}^{ign}$$

$$\dot{y} = A_{11}y + A_{12}q + B_1\hat{u}_{ROO-SMC}^{ign}$$

$$\hat{z} = Mw + (P + ML)y$$

Suppose that (A, C) is detectable and $(A - LC)$ is Hurwitz. The estimated sliding mode reduced order control law with sign function is guaranteed an *asymptotically stable* for the system (2)

$$\hat{u}_{ROO-SMC}^{ign}(t) = -[RGK_1 w + RGK_2 y + RGK_3 q] \text{ sign}(\sigma(\hat{z}))$$

where,

$$RGK_1 := [G_{ss}^T (MB_2 + PB_1)]^{-1} G_{ss}^T (MA_{22} - MLA_{12})$$

$$RGK_2 := [G_{ss}^T (MB_2 + PB_1)]^{-1}$$

$$G_{ss}^T [M(A_{22} - LA_{12})L + MA_{21} + PA_{11}]$$

$$RGK_3 := [G_{ss}^T (MB_2 + PB_1)]^{-1} G_{ss}^T (P + ML)A_{12}$$

subject to $\text{sign}(\sigma(\hat{z})) = 1$ for $\sigma(\hat{z}) > 0$

$$\text{sign}(\sigma(\hat{z})) = 0 \quad \text{for } \sigma(\hat{z}) = 0$$

$$\text{sign}(\sigma(\hat{z})) = -1 \quad \text{for } \sigma(\hat{z}) < 0$$

Proof. Let us define the estimation error and the differential estimation error

$$e = z - \hat{z}$$

$$\dot{e} = \dot{z} - \dot{\hat{z}} = A_{22}q + A_{21}y + B_2\hat{u}_{ROO-SMC}^{ign} - (A_{22}\hat{q} + A_{21}y + B_2\hat{u}_{ROO-SMC}^{ign})$$

$$+ L(\dot{y} - A_{11}y - B_1\hat{u}_{ROO-SMC}^{ign} - A_{12}\hat{q})$$

$$= (A_{22} - LA_{12})(q - \hat{q}) = (A_{22} - LA_{12})e$$

Lyapunov's function candidate is chosen by

$$V = \frac{1}{2}\sigma^T\sigma + \frac{1}{2}e^T e$$

The derivative of a Lyapunov's function is

$$\begin{aligned}\dot{V} &= \sigma^T \dot{\sigma} + e^T \dot{e} = \sigma^T \left(G_{ss}^T \dot{\hat{z}} \right) + e^T (A_{22} - LA_{12})e \\ &= \sigma^T \left(G_{ss}^T (M\dot{w} + (P + ML)\dot{y}) \right) + e^T (A_{22} - LA_{12})e \\ &= \sigma^T \left(G_{ss}^T M(A_{22} - LA_{12})w + G_{ss}^T ((MA_{22} - MLA_{12})L \right. \\ &\quad \left. + (MA_{21} + PA_{11}))y + G_{ss}^T (P + ML)A_{12}q \right. \\ &\quad \left. - (G_{ss}^T MB_2 + G_{ss}^T PB_1) (RGK, w + RGK, y \right. \\ &\quad \left. + RGK, q) \text{sign}(\sigma(\hat{z})) \right) + e^T (A_{22} - LA_{12})e \\ \dot{V} &= \sigma^T \left[G_{ss}^T M(A_{22} - LA_{12})w + G_{ss}^T ((MA_{22} - MLA_{12})L \right. \\ &\quad \left. + (MA_{21} + PA_{11}))y + G_{ss}^T (P + ML)A_{12}q \right. \\ &\quad \left. - (G_{ss}^T MB_2 + G_{ss}^T PB_1) \left[G_{ss}^T (MB_2 + PB_1) \right]^{-1} \right. \\ &\quad \left. G_{ss}^T (MA_{22} - MLA_{12})w \text{sign}(\sigma(\hat{z})) \right. \\ &\quad \left. - (G_{ss}^T MB_2 + G_{ss}^T PB_1) \left[G_{ss}^T (MB_2 + PB_1) \right]^{-1} \right. \\ &\quad \left. G_{ss}^T [M(A_{22} - LA_{12})L + MA_{21} + PA_{11}]y(t) \text{sign}(\sigma(\hat{z})) \right. \\ &\quad \left. - (G_{ss}^T MB_2 + G_{ss}^T PB_1) \left[G_{ss}^T (MB_2 + PB_1) \right]^{-1} \right. \\ &\quad \left. G_{ss}^T (P + ML)A_{12}q \text{sign}(\sigma(\hat{z})) \right] + e^T (A_{22} - LA_{12})e\end{aligned}$$

Let $G_{ss}^T (MB_2 + PB_1) \left[G_{ss}^T (MB_2 + PB_1) \right]^{-1} = I$,

$$\begin{aligned}\dot{V} &= \sigma^T \left[G_{ss}^T M(A_{22} - LA_{12})w \right. \\ &\quad \left. + G_{ss}^T ((MA_{22} - MLA_{12})L + (MA_{21} + PA_{11}))y \right. \\ &\quad \left. + G_{ss}^T (P + ML)A_{12}q - G_{ss}^T (MA_{22} - MLA_{12})w \text{sign}(\sigma(\hat{z})) \right. \\ &\quad \left. - G_{ss}^T [M(A_{22} - LA_{12})L + MA_{21} + PA_{11}]y \text{sign}(\sigma(\hat{z})) \right. \\ &\quad \left. - G_{ss}^T (P + ML)A_{12}q \text{sign}(\sigma(\hat{z})) \right] + e^T (A_{22} - LA_{12})e \\ &= \sigma^T G_{ss}^T M(A_{22} - LA_{12})w (1 - \text{sign}(\sigma(\hat{z}))) \\ &\quad + \sigma^T G_{ss}^T (P + ML)A_{12}q (1 - \text{sign}(\sigma(\hat{z}))) \\ &\quad + \sigma^T G_{ss}^T (M(A_{22} - LA_{12})L + MA_{21} + PA_{11})y (1 - \text{sign}(\sigma(\hat{z}))) \\ &\quad + e^T (A_{22} - LA_{12})e\end{aligned}$$

If $(A_{22} - LA_{12})$ is stable, the estimation error is $e \rightarrow 0$ as $t \rightarrow \infty$.

$$\begin{aligned}\dot{V} &= \sigma^T G_{ss}^T M(A_{22} - LA_{12})w (1 - \text{sign}(\sigma(\hat{z}))) + \sigma^T G_{ss}^T (P + ML) \\ &\quad A_{12}q (1 - \text{sign}(\sigma(\hat{z}))) + \sigma^T G_{ss}^T (M(A_{22} - LA_{12})L \\ &\quad + MA_{21} + PA_{11})y (1 - \text{sign}(\sigma(\hat{z}))) \leq 0\end{aligned}$$

subject to, if $\sigma > 0$, $\dot{V} = 0$
if $\sigma = 0$, $\dot{V} = 0$
if $\sigma < 0$, $\dot{V} = 2kG_{ss}^T M(A_{22} - LA_{12})w$
 $+ 2kG_{ss}^T (P + ML)A_{12}q$
 $+ 2kG_{ss}^T (M(A_{22} - LA_{12})L + MA_{21} + PA_{11})y < 0$

where, k is positive constant. The above condition is satisfied on negative definite, and is *asymptotically stable*. This completes the proof of this theorem. \square

3. Conclusion

A nonlinear feedback linearization-reduced order observer-based sliding mode controller (NFL-ROO-based SMC) has been proposed and a stability proof of a closed-loop system has been done.

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