

# Point of Soft Switching Technology on Practical Application

Takashi Koga (Koga Engineering)\*

## Abstract:

Remarkable progress has been performed in power electronics, using high frequency switching based on the improvement of power semi-conductor devices. In the other hands, it gives us serious problems, such as, insulation, increasing of the high frequency leakage current, and electric corrosion of bearing in the loaded motors driven by inverters using high frequency switching. To improve these problems, many researches have made especially on the application of soft switching technologies. From this point of view IEE-Japan had started the research groups on soft-switching technology 1997 and 1999. This paper is a survey based on the discussion in this research group with results of ARCP inverter applied for 210kVA power supply.

Keyword : Soft Switching, ARCP-Inverter, Auxiliary Power Supply, SI-Thyristor

## 1. Introduction

In the field of power electronics, it is realized to get high performance using high frequency switching, based on improvement of power semiconductor devices as IGBT. It gives us many remarkable contributions not only for power conversion also for many industrial systems like vector control which gives us new filed on motor drive system.

This high frequency switching gives us higher  $dv/dt$  on the out put pulse in the same time. As a results of this high frequency switching, we have met serious problems like failure of insulation, increasing of high frequency leakage current, and sometimes electric corrosion of bearing in loaded motors. [1]-[7]

Soft switching technology is very effective for these problems and reduction of switching loss in devices also, so there are many researches and trials.[8]-[11]

From this point of view IEE-Japan had established the research committee on soft-switching technology 1997 and extension 1999. In this paper, I will introduce major soft switching technologies applicable for high power converter, based on the survey made by this committee, with a practical result of ARCP (Auxiliary resonant commutation pole) inverter which was developed for railway motor couch as auxiliary power supply by Toyo Electric Mfg. Co., Ltd. [38]

## 2. Circuit topologies proposed for this use

### 2-1 General review

Soft switching are applied for DC/DC converters of small power range widely, however, there are many difficulties on the application for high power equipment, for instance, increasing of peak stress for main devices, increasing of the power loss in

resonance circuits, difficulty to meet controllability required from high class application and so on.

There are proposals using adjustment of the gate drive current for IGBT, or make some arrangement on snubber circuit in smaller power converter. However, it is necessary to make up soft switching by main circuits configuration in high power converters.

From these points of view there are many proposals as follows:

#### (a) Resonant DC link methode

To get ZVS(zero volt switch) or ZCS(zero current switch) by oscillation of input DC current or voltage.

#### (b) Commutation using inductor

To get soft switching using loss less snubber in turn-off state, and current suppression effect by inductance which added to main circuit, in turn-on state.

#### (c) Partial resonance inverter

To make resonance when the device is turn on or turn off stages only.

### 2-2 Parallel resonant DC link method

Fig.2-1 shows proposal of parallel resonant DC link inverter which has resonant circuit by  $L$ , and  $C$ , in DC stage and makes ZVS or ZCS in main devices when the DC voltage is zero by the resonance circuit operation. [15]

In this proposal it is possible to use main devices in stead of device  $T_c$ .

In this topology has merits as follows;

- (1) No switching loss in main devices.
- (2) No higher frequency than resonant frequency.
- (3) Need not use snubber circuit.

However has some disadvantages as follows,

- (a) Peak voltage up to 2 times of power supply or more by resonance.

- (b) Big power dissipation in resonance circuit at partial load operation.

\* Takashi KOGA : Invited Professor  
Kyunqnam University. Masan. KOREA

- (c) In this topology the output power is adjusted by PDM (pulse density modulation), so it is necessary to use very high frequency than output frequency to get wide control range.
- (d) Difficult to get good distortion factor in output current.

To improve these disadvantages there are some proposals for suppression of peak device stress by adding auxiliary circuit like fig.2-2. [16][17] By this improvement the peak voltage of DC stage  $V_{cmmax}$  is clamped to original voltage of  $E_{dc} + V_{cc}$  (voltage of capacitor  $C_c$ ). However, it requires additional control for this circuit and gives us additional loss in added circuits,

### 2-3 Commutation using inductor

Fig.2-3 shows an example of this proposed circuit.[18][19] In this circuit the waveform of the output terminals between  $u$ ,  $v$ , and  $w$  are pulses modulated by PWM, but output waveforms between terminals of capacitor  $C_{zc}$  are in sinusoidal waves.

In this proposal there is no resonance circuit, however, it is possible to get soft switching by loss less snubber of  $C_{R1}$ ,  $C_{R1}'$  at turn off, by inductors  $L_{zc}$  at turn on.

In this circuit the output current is limited less than circulating current. If we use conventional PWM control using constant carrier frequency, it request us big circulating current in spite of partial loaded condition or lower modulation factor.

As improvement, it is proposed to modulate the carrier frequency sinusoidal, to higher frequency in small output and to lower in high output.[20]

### 2-4 Partial resonance inverter

#### (1) Partial resonance inverter by passive element

Fig.2-4 shows resonant pole inverter.[21] Adding resonant reactor  $L_r$  and resonant capacitor  $C_{Fi}$  soft switching are performed in main devices, by the partial resonance with loss less snubber capacitors  $C_{r1}, C_{r2}'$ .

In this circuit to get soft switching, it is necessary to be negative current in inductor when main switches turn on. As a results large current of inductor is requested, it gives us higher loss. AS improvement, it is proposed to use variable hysteresis band in PWM control comparator.

Fig.2-5 shows resonant diode pole inverter, improved circuit of above circuit shown in fig.2-6, by adding diodes for voltage clamping and free wheeling of load current. [22]

Although it is available to get good partial resonance by this circuit, in the same time gives us some drawbacks as follows;

- (a) Big resonance current is needed in smaller load operation.

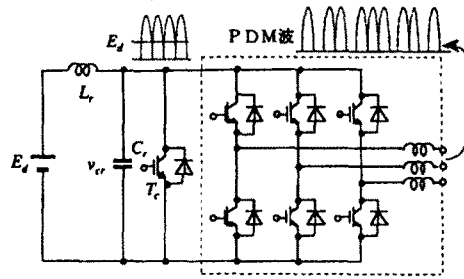


Fig.2-1 Parallel resonant DC link Inverter

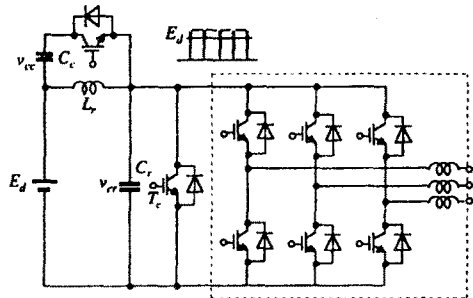


Fig.2-2 Parallel resonant DC link Inverter with voltage clamp

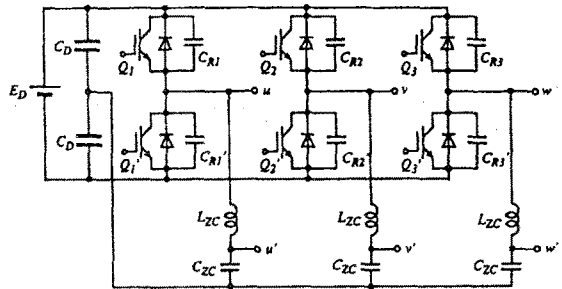


Fig.2-3 Inductor commutation inverter

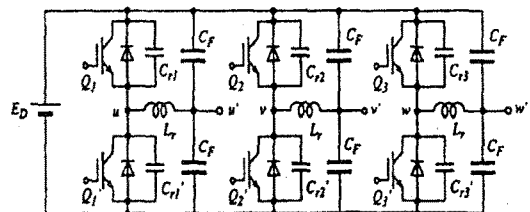


Fig.2-4 Resonant pole inverter

- (b) By the overlapping of load current and resonance current, loss of reactor  $L_r$  is high.
- (c) There are some difficulties in keeping of resonant condition or increasing of resonant current by power line voltage disturbances.

(d) Difficult to keep soft switching condition in heavy load

To improve these problems remarkable idea using current transformer shown in fig.2-6 was proposed. [23] This circuit gives us good result by adding passive elements only. However, there is remaining one problem that this circuit requires big size current transformer.

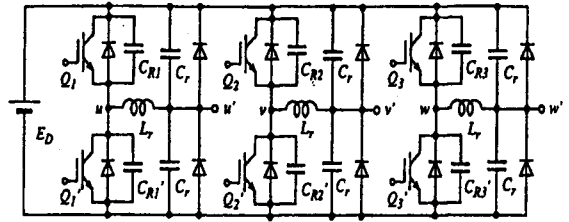


Fig.2-5 Resonant diode pole inverter

(2) Partial resonance DC link inverter

Fig.2-7 shows an example of partial resonant DC link inverter. We can get partial resonance by adding resonance circuit shown in figure. [24]

By turning on  $T_{r1}$  and  $T_{r2}$  in the same time, initial current flows through  $T_s$ , and by turning off of  $T_s$  the voltage of  $C_r$  goes down to zero. To change off on-devices at inverter, they are switched in the interval of zero voltage. By turning off of  $T_{r1}, T_{r2}$ , current of reactor  $L_r$  flows through diodes  $D_{r1}, D_{r2}$  and charge up capacitor  $C_r$ . After the voltage of  $C_r$  goes higher than supply voltage, the current flows to power supply through diode  $D_s$ , and the voltage of  $C_r$  is kept to the same voltage of power supply. Then ZVS of  $T_s$  is performed. By turning on of  $T_s$ , the current of reactor  $L_r$  degrades to zero and after it diodes  $D_{r1}, D_{r2}$  are turn off. There is no switching loss at turning off of  $T_s$ , because this turn off is performed at the period of the voltage of  $C_r$  is equal to power supply.

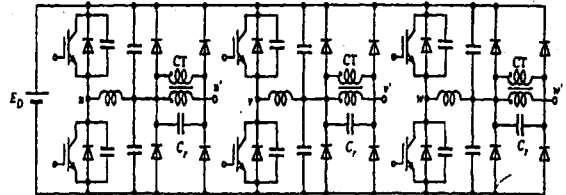


Fig.2-6 Resonant diode pole inverter with current transformer

There are many proposals about this partial resonance DC link inverter, and many additional improvement also. [25][26]

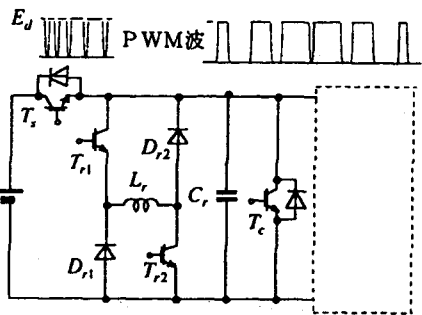


Fig.2-7 Partial resonance DC link inverter

(3) ARCP(Auxiliary resonant commutation pole) inverter

In this strategy partial resonance is performed by using auxiliary resonant circuits added to each phase circuits. Detail explanation is in next chapter.

2-5 Soft switching inverter using resonant circuits added to AC output

Fig.2-8 shows an example of this proposal. [27] In this topology the adjustment of output is performed by PDM(Pulse density modulation).

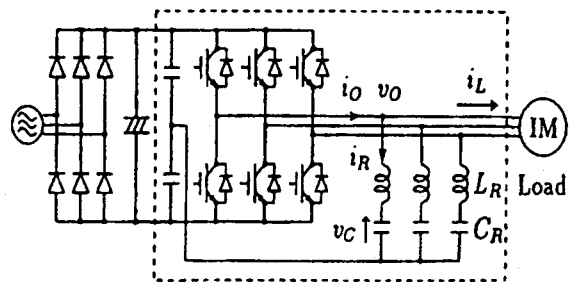


Fig.2-8 Soft switching inverter with AC side resonant circuits

2-6 Conclusion of this chapter

As mentioned above, there are many proposals in soft switching inverter especially for higher output power. They have features in its way and disadvantages in the same time. It is difficult to find out one circuit suitable for all applications. It is very important to select the most suitable topology for each application based on design assessment.

3. ARCP inverter

3-1 Fore word

This concept is based on the proposal made by Dr. W. Mc Murray. [28] In this topology, partial resonance are performed by the operation of resonance circuits added to each phase. Although the circuit configuration is complex, it is possible to get good resonance condition in wide operation range, and to reduce peak stress of main devices.

there are many papers and proposals of improvement [29], applications [30][32], reduction of loss [31], and so on.

### 3-2 Basic circuit configuration

In this topology we add resonance circuits which are constructed by auxiliary devices  $S_{A1}$ ,  $S_{A2}$  to each phase as shown in fig. 3-1. In this figure,  $C_{r1}$ ,  $C_{r2}$  and  $L_r$  are resonance capacitors and reactor.

$C_1$ ,  $C_2$  are used for keeping of neutral potential and for filter capacitor in DC stage.

Fig.3-2 shows operating waveforms of important position in this circuit. And fig.3-3 shows operation modes about this circuit.

From these figures:

Mode I : ( $\sim t_0$ )

This is a steady state mode before output voltage changes from negative to positive. By the lagging load current, the load current flows through diode  $D_2$  not main device  $S_2$ . Resonant capacitor  $C_{r1}$  is charged up to  $E$ ,  $C_{r2}$  is discharged to zero.

Mode II : ( $t_0 \sim t_1$ )

In the condition diode  $D_2$  conducting, drive  $S_{A1}$  to turn on and gate off for  $S_2$ .  $S_2$  is turned off in ZCS, and  $S_A$  turns on in ZCS by suppression effect of reactor  $L_r$ . Increasing of reactor current  $i_r$  and after current of  $D_2$  is zero, load current  $I_0$  is held by  $i_r$ .

Mode III : ( $t_1 \sim t_2$ )

This region is in recovery condition of  $D_2$ .

Mode IV : ( $t_2 \sim t_3$ )

The resonance starts in fig.3-2 the voltage of  $C_{r1}$  is clamped to zero by  $D_1$ .

Mode V : ( $t_3 \sim t_4$ )

In the interval of  $i_r$  decreasing,  $S_1$  is turns on in the condition of ZCS and ZVS.

Mode VI : ( $t_4 \sim t_5$ )

Difference current of  $i_r$  from  $I_0$  is supplied from  $S_1$ , at a results  $i_r$  goes to zero.

Mode VII : ( $t_5 \sim t_6$ )

When current of  $i_r$  is zero, load current  $I_0$  is supplied by  $S_1$  and change to steady state.

Mode VIII : ( $t_6 \sim t_7$ )

In this mode,  $S_1$  goes to off, and  $S_2$  to on. By turn off of  $S_1$  the current of  $I_0$  is divided to two current for  $C_{r1}$  and  $C_{r2}$ , as a results AC output voltage is automatically changes its polarity. Although it needs not to operate resonance circuit, it is better to use auxiliary resonance commutation to accelerate the commutation in partial load condition.

At moment of  $t_6$ , make turn off of  $S_1$  and

turn on of  $S_{A2}$  in the same time. By the turn off of  $S_1$ , current of  $I_0$  is commutated to  $C_{r1}$ , and  $C_{r2}$ , then ZVS is performed.

(In practice there is some loss by the

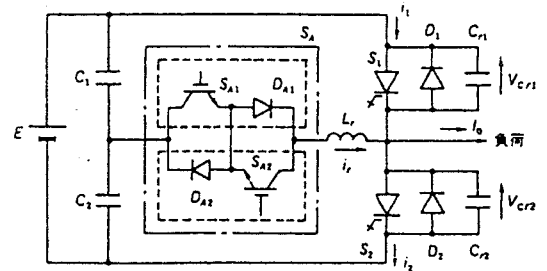


Fig.3-1 ARCP Inverter(1 phase)

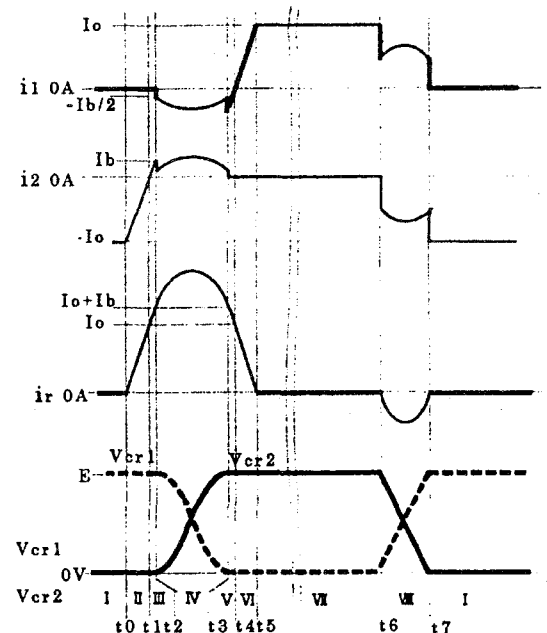


Fig.3-2 Commutation wave forms in ARCP Inverter

tailing current)

Mentioned above, in this topology it is possible to make ZCS and ZVS in main devices by partial resonance, as a result, it is possible to reduce switching loss of main devices, and to keep good resonant condition in spite of lode variation.

## 4. Practical application of ARCP inverter

### 4-1 Back ground

In conventional railway DC1500V is used widely for power supply. It is requested to have good inverter for many equipment of air conditioners, lights, power supply for controllers and so on.

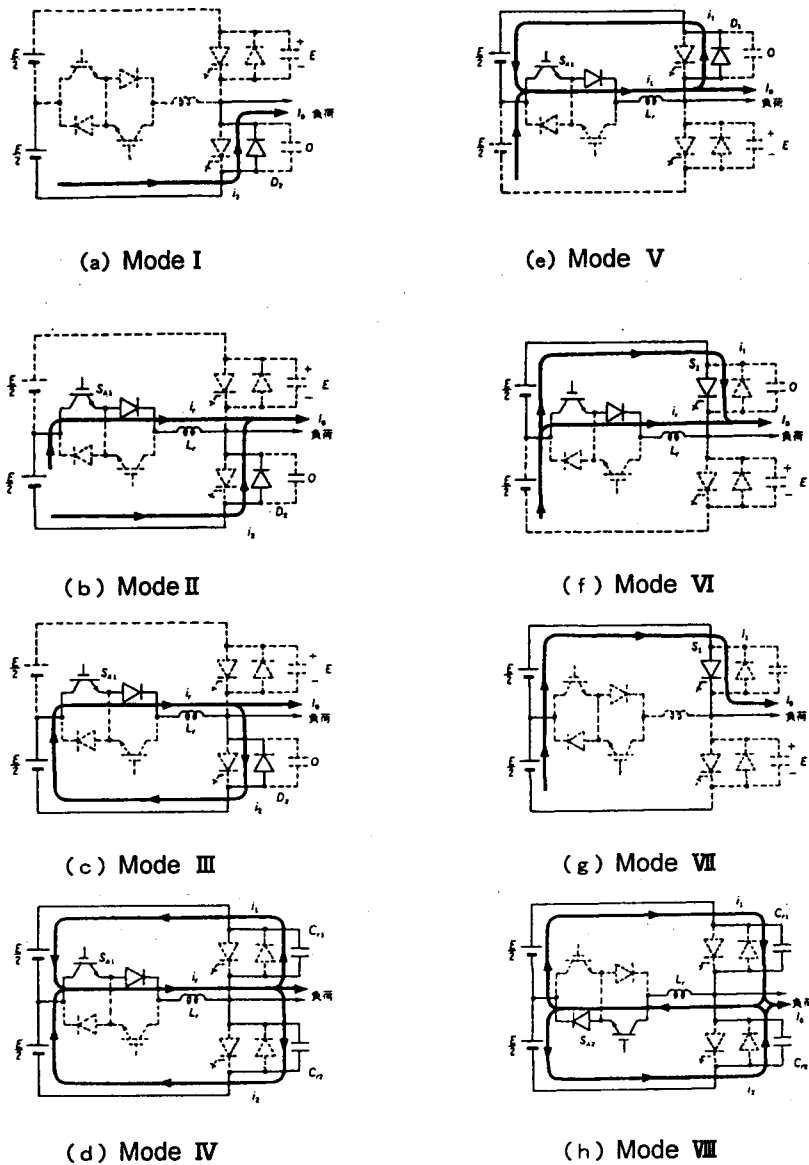


Fig. 3-3 Commutation in ARCP Inverter

The voltage of the feeder line has wide deviation caused by load condition, distance from substation, and re-generation seriously. The voltage is change from 900V to 2000V sometimes. For this situation, the auxiliary power supply is requested to have good waveform, excellent stability against the change of the load and feeder voltage including transient also. As the auxiliary power supply is usually used 1-set for 3 or 4 coaches, the power capacity is needed over 200kVA. For these requirements high frequency switching is very effective, but there are some difficulties for the application of high voltage devices.

Additionally in railway system many high frequency currents are used in signal system. From this situation it is requested with high importance to reduce the noise level in rail circuit.

From these points of view we tried to make excellent inverter using soft switching, by simple 2-level inverter.

#### 4-2 Specification of the developed inverter

##### (1) Specification

Table 4-1 shows the specifications. For the practical long period working test, out side style was arranged to the same size with practical equipment. [33][34]

Table 4-1 Specification of development

Items	Specification
Main circuit	ARCP 3Phase PWM Inverter
Control	Instantaneous Space Vector
input Voltage	DC 1500V
Workable	DC 900 - 1800V
Rated output	3 $\phi$ 60Hz 440v 210kVA
Regulation	less than +/- 2%
Distortion	less than 2%

## (2) Constructions

Main circuits are shown in fig.4-1. The resonance circuits are the same with  $S_A$  in fig.3-1. We chose for main devices SI-Thyristor having 4kV 2kA turn off 2 s, for auxiliary switch IGBT of 400A by natural convection cooling with heat pipe radiator.

We chose 100kHz for the resonant frequency, 5.4kHz for carrier frequency. As a results, remarkable reduction of size and weight is performed.

## 4-3 Experimental results

Regulation, efficiency, and some waveforms are shown in fig. 4-2 to 4-5. By these development we could get good waveform distortion less than 1.1%, good dynamic performances, and excellent noise reduction highly appreciated by signal system.

This equipment were installed to the normal operating coach in Nanbu line of JR-East Japan at 1998, and confirmed its excellent utility by practical operation.

## 5. Important points for soft switching application

### 5-1 Choice of circuit configuration

Obviously this is the most important subject. As there is no one circuit best for all application, it is necessary to select the most suitable circuit for the application with careful assessment not only typical performance but also in the detail of practical operation.

### 5-2 Loss of the resonant circuit

In resonant circuit the peak current is extremely high, sometimes in partial load also. The important subject is reduction of loss in resonant circuit.

### 5-2 Characteristics of main device

One of important points is tailing current of the devices in the application of soft switching, especially in high power application. It is said that thyristors are more suitable for resonant soft switching, like GCT or SI-Thyristor. The characteristics of the devices should be check

carefully more than conventional equipment using hard switching. [35]

## 6. Conclusion

Based on the research of the committee and practical results of ARCP inverter, I had reported review of soft switching strategies and important points for high power application.

Today we have met serial problems based on high frequency switching in the practical field. The soft switching is very important for these problems, but it is not so easy to apply for practical equipment effectively.

I hope to get good solution in near future by co-operation of device engineers and circuit engineers.

## Acknowledgement

This paper based on the results of the research committee of IEE Japan, and also Dr. K.Ihda and Mr.K.Harada in charge of development for AIECP-Inverter in Toyo Electric Mfg. Co. Ltd. I express many thanks for those people.

## [Reference]

- [1] 今柳田ほか [一般産業システムにおける高効率化と高調波抑制技術] 電学産業応用部門大会 S4-5, 1998年8月
- [2] 小笠原 [可変速ACドライブの洩れ電流・サージ電圧・軸電圧とその抑制法] 電学論 Vol.118-D, No.9, pp975-980, Sept.1998
- [3] 赤木ほか [電圧型PWMインバータが発生する高周波洩れ電流の特性と理論解析] 電学論 Vol.115-D No.1, pp77-83 Jan.1995.
- [4] 土屋ほか [電圧型インバータ波形による低圧絶縁の複合劣化] 東洋電機技報 第8, pp13-19 1993年6月
- [5] 電学調査委編 [パワーエレクトロニクス機器の電磁波ノイズ] 電気学会技術報告 第545号 1995年5月
- [6] 黒木ほか [電力変換装置より放射される電磁ノイズの解析] 電学産業応用部門大会 No.82, 1997年8月
- [7] D.McDonald et al. [PWM Drive Related Bearing Failures] IEEE IA Magazine pp41-47 July/Aug. 1999
- [8] 長尾 [インバータのソフトスイッチング化について] 熊本工大エレクトロニクス研究所報告 Vol.13, No.1, pp36-41, 1997.
- [9] 谷口 [共振型インバータ回路方式の動向] 電学論 Vol.117-D, No.2, Feb. 1997年
- [10] 電学調査専門委編 [電力変換器の高性能スイッチング技術] 電気学会技術報告 第687号 1998年8月
- [11] 佐藤ほか [共振DCリンクインバータの解析と制御法の改善] 電学論 Vol.111-D, No.7, pp531-539, July, 1991.
- [12] 電学委 [高周波共振型スイッチング電源方式と応用技術の動向] 電学技術報告II部 第443号 1992年11月
- [13] 滝沢 [低ノイズ・スパンノイズ化を実現するIGBT用ゲート駆動回路] 電学研 SPC96-111, 1996.
- [14] 山田 [PWMコンバータ・インバータシステムにおけるスイッチング波形改善方法] 電学研 SPC96-120, 1996.
- [15] D.M.Divan et al. [The Resonant DC-Link Converter-A New Concept in Static Power Converter] IEEE IAS Ann.Meeting, pp648-656, Oct.1986
- [16] 村井 [高周波共振を応用した半導体電力変換技術] 電学論 Vol.110-D, No.1, pp43, Jan. 1990.
- [17] D.M.Divan [Zero-Switching-Loss Inverter for High Power Applications] IEEE T-IAS, Vol.25, No.4, July.1989

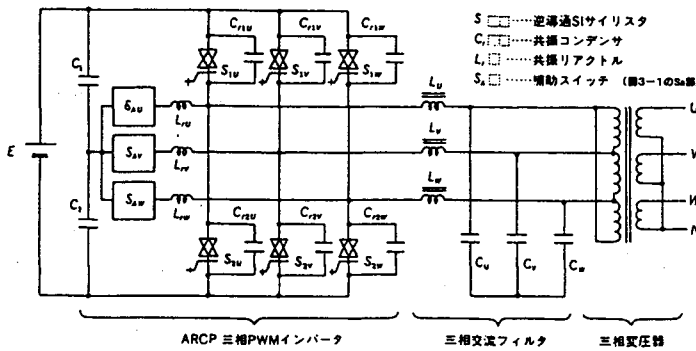


Fig.4-1 ARCP Inverter for auxiliary power supply  
(Input DC1500V Output 3φ 440V 210kVA)

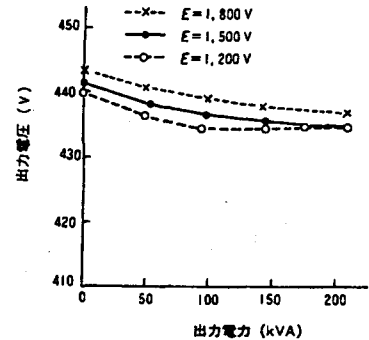


Fig.4-2 Regulation of output voltage

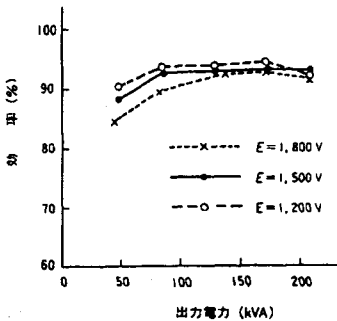
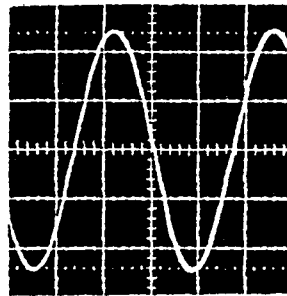
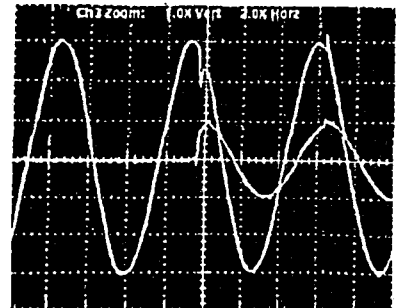


Fig.4-3 Efficiency against to output power



全負荷時 250 V/div 5ms/div

Fig.4-4 Wave form of output voltage in full load



全負荷投入時波形 200V/div.

fig.4-5 Wave forms on transient at full load on

- [18] 長尾ほか [ゼロ電流ターンオフ高キャリア周波数 PWM インバータ] 電学研 SPC92-67, 1992年10月
- [19] 長尾, 原田 [デッドタイムによる波形歪みをなくした非共振型 PWM インバータ] 電学論 Vol. 114-D, No. 2, pp129-136, Feb. 1994.
- [20] 長尾, 原田 [インダクタ転流ソフトスイッチング PWM インバータのキャリア周波数変調による効率改善] 信学論 C-2, Vol. J79-C2, No. 5, pp161-169, May, 1996.
- [21] G. Cho, et. al [Three Phase Sine Wave Voltage Source Inverter using Soft Switched Resonant Poles] IECON89, Nov. 1989.
- [22] Al-Haddad, [A Rugged Soft Commutated PWM Inverter for AC Drive] PESC90 pp656-662, June 1990
- [23] 松尾, 黒川 [AC カレントランスを持つソフトスイッチング方式 PWM インバータについて] 信学論 B-1, Vol. J80-B1, No. 11, pp1-7, Nov. 1997
- [24] J. G. Cho, [Novel soft Switching PWM Converter using New Parallel Resonant DC Link] PESC91, No. 241, 1991
- [25] Taniguchi et al. [A PWM Method for Quasi Resonant ZVS Inverter] EPE93, Proc. 3, No. 377, Oct. 1993
- [26] 村井ほか [部分共振電流型 PWM インバータの出力特性の検討] 電学論 Vol. 118-D, No. 3, pp345-352, Mar. 1998.
- [27] 赤木 [交流側に共振回路を接続した ZCS 3 相 PWM インバータの制御法と動作特性] 電学論 Vol. 118-D, No. 6, June, 1998
- [28] W. McMurray [Resonant Snubbers with Auxiliary Switches] IEEE IAS Ann. Meeting, pp829-834, Oct. 1989
- [29] R. W. De Doncker [The Auxiliary Resonant Commutated Pole Converter] IEEE IAS Ann. Meeting, pp1228-1235, Oct. 1990
- [30] 近藤 [補助共振転流ボーム型インバータにおける電磁放射ノイズと効率の評価] 電学論 Vol. 116-D, No. 4, pp499, April. 1996.
- [31] 木村 [補助共振転流ボーム型 PWM インバータの損失最小化条件と実用上の問題点] 電学論 Vol. 118-D, No. 3, pp385-392, March. 1998.
- [32] H. Matsuo et al. [High Power Soft Switching PWM AC Auxiliary Power Supply System of The Electric Railway Rolling Stock and its Deadbeat Control] PESC-85, pp258-263, June. 1985
- [33] 原田 [SI サイスタによる部分共振型正弦波 PWM インバータと制御法] 東洋電機技報 第 94 号 pp2-12, 1994 年 4 月
- [34] K. Iida et al. [210kVA Soft Switching PWM AC Auxiliary Power Supply System of The Electric Railway Rolling Stock using an ARCP Inverter] IPEC95 pp831-836, 1995
- [35] K. Iida et al. [A Novel Firing Control and Over Current Protection of the Main Power Switches in the ARCP 3 Phase Inverter] PESC98 pp594-599, 1998.
- [36] 佐久間他 [補助共振転流ボームインバータにおける配線インダクタンスの影響] 電学産業応用部門大会 265, pp255-258, 1996
- [38] 古賀, 黒川 他 [ソフトスイッチングインバータの実用化と問題点] 電学研 SPC99-120, 1999