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Compliant Stage for Nano Patterning Machine

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Key Words: Nano pattern(), Nano imprint(), Lithography(),

Compliant stage ()

The nano imprint process is one of the next generation lithography has been mentioned as one of major nanoreplication techniques because it is simple process, low cost, high replication fidelity and relatively high throughput. This process requires a surface contact between a template with patterns and a wafer on a stage. After contact, the vertical moving the template to the wafer causes some directional motions of the stage. Thus the stage must move according to the motions of the template to avoid the damage of the transferred patterns on the wafer. This study is to develop the wafer stage with a passive compliance to overcome the damage. This stage is designed with the concept like that it has a monolithic, symmetry and planar 6-DOF mechanism.

Abstract

1. 가 IT NT 1995 Chou 가 가 100 ArF , 2007 45 nm nm , 10 nm (1) 가 6 (Imprint lithography) 가 2. 2.1 Fig.1 E-mail: kbchoi@kimm.re.kr (2) (Transfer layer) TEL: (042)868-7135 FAX: (042)868-7135

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(Quartz) 기

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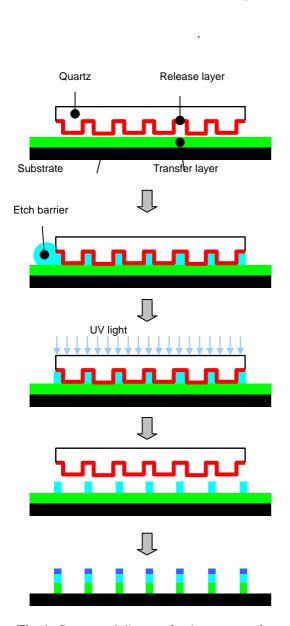


Fig. 1 Conceptual diagram for the process of a nano imprint lithography

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Fig. 2

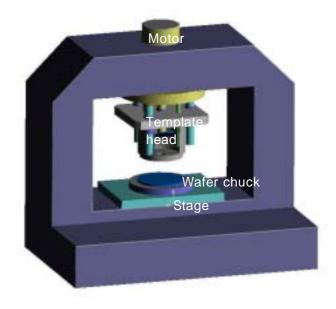


Fig. 2 Structure of a nano imprint machine

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Fig. 3

가 가 2 가 (center) 가 4. 가 5 가 0, 2 가 3 1, (Out-of-motion) 1, 2, 3 (In-plane motion) 4, 5, 6, 7, 8, 9

 $\mathbf{M}\ddot{\mathbf{q}} + \mathbf{K}\mathbf{q} = \mathbf{0} \tag{1}$

, $\mathbf{M} = \begin{bmatrix} \mathbf{M}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{M}_2 \end{bmatrix}$ (2) Fig. 3 . $\mathbf{M}_i = dia \begin{bmatrix} m_i & m_i & m_i & I_{vi} & I_{vi} & I_{vi} \end{bmatrix}$ (3)

 $\mathbf{M}_{i} = dia \begin{bmatrix} \mathbf{m}_{i} & \mathbf{m}_{i} & \mathbf{m}_{i} & \mathbf{I}_{xi} & \mathbf{I}_{yi} & \mathbf{I}_{zi} \end{bmatrix}$ (3) $\mathbf{K} = \begin{bmatrix} \mathbf{K}_{11} & -\mathbf{K}_{12} \\ -\mathbf{K}_{21} & \mathbf{K}_{22} \end{bmatrix}$ (4)

 $\mathbf{K}_{11} = \sum_{j=1}^{9} \widetilde{\mathbf{D}}_{1j} \widetilde{\mathbf{K}}_{j} \widetilde{\mathbf{D}}_{1j}^{T}$ (5)

 $\mathbf{K}_{22} = \sum_{j=1}^{9} \widetilde{\mathbf{D}}_{2j} \widetilde{\mathbf{K}}_{j} \widetilde{\mathbf{D}}_{2j}^{T}$ (6)

 $\mathbf{K}_{12} = \mathbf{K}_{21} = \sum_{i=4}^{9} \widetilde{\mathbf{D}}_{1j} \widetilde{\mathbf{K}}_{j} \widetilde{\mathbf{D}}_{2j}^{T}$ (7)

 $\mathbf{D}_{ij} = \begin{bmatrix} 0 & -d_z & d_y \\ d_z & 0 & -d_x \\ -d_y & d_x & 0 \end{bmatrix}_i$ (8)

 $\widetilde{\mathbf{K}}_{i} = \begin{bmatrix} {}^{O}\mathbf{R}_{O_{si}} & \mathbf{0} \\ \mathbf{0} & {}^{O}\mathbf{R}_{O_{si}} \end{bmatrix} \widetilde{\mathbf{K}}_{si} \begin{bmatrix} {}^{O}\mathbf{R}_{O_{si}} & \mathbf{0} \\ \mathbf{0} & {}^{O}\mathbf{R}_{O_{si}} \end{bmatrix}^{T} (9)$

Fig. 3 Structure of a stage with flexure

. ${f D}$. ${f \widetilde K}_{si}$. i (stiffness) , ${}^o{f R}_{O_{si}}$. i . $(1)\sim(9)$

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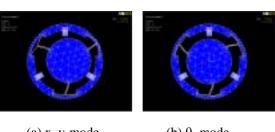
 $f = [66.7 \ 66.7 \ 64.5 \ 129.8 \ 129.8 \ 114.5] (10)$ **FEM**

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Fig. 4



(a) x, y-mode

(b) θ_z mode

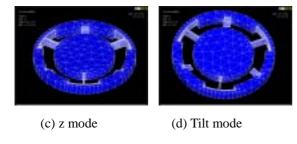


Fig. 4 Simulation results of modal analysis

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