

한국소성가공학회 2004년도 금형가공-신포자연

플라스틱 거푸집 패널의 성형특성에 관한 기초 연구

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토목구조물의 플라스틱대체 기초성형기술개발

- 고분자 플라스틱 재료는 재활용이 가능한 친환경적인 소재임.
- 고분자 제품의 성형시 크기가 기존의 제품대비 상대적으로 커지게 되면 수축 및 수축편차로 인한 **휨 현상**(휨 현상)이 더욱 크게 발생함.
- 제품의 휨에 영향을 주는 인자는 크게 **Material, Part Design, Tooling & Processing Parameter**로 구분될 수 있음.
- **Material** 측면에서는 하중을 받는 부재 이므로, 강성 증가를 위한 **Fiber Filled** 수지가 사용됨.
- **Part Design** 측면에서는 **구조설계** 상 여러 가지 보강 현상이 존재 하지만 기본적인 구조는 사전에 결정되어 있음(1800x600x4mm, 1200x600x4mm).
- 따라서 본 연구에서는 변경이 가능한 **Tooling & Processing Parameter** 및 성형공법 자체의 변화를 통해 대형 직교 보강 플라스틱 평판의 성형특성에 관한 기초 연구를 수행하고자 함.

Air Trap

Overpacking

Hesitation

Thick/thin

Gating/Packing

Weld/Meld lines

Part

Design

Tooling

Parameters

Short Shot
Sink Mark

Flash

Flow Mark

Silver Streak

Gloss badness

Cracking

Voids

Jetting

Strength, etc.

Gate Selection

Gate Sizing

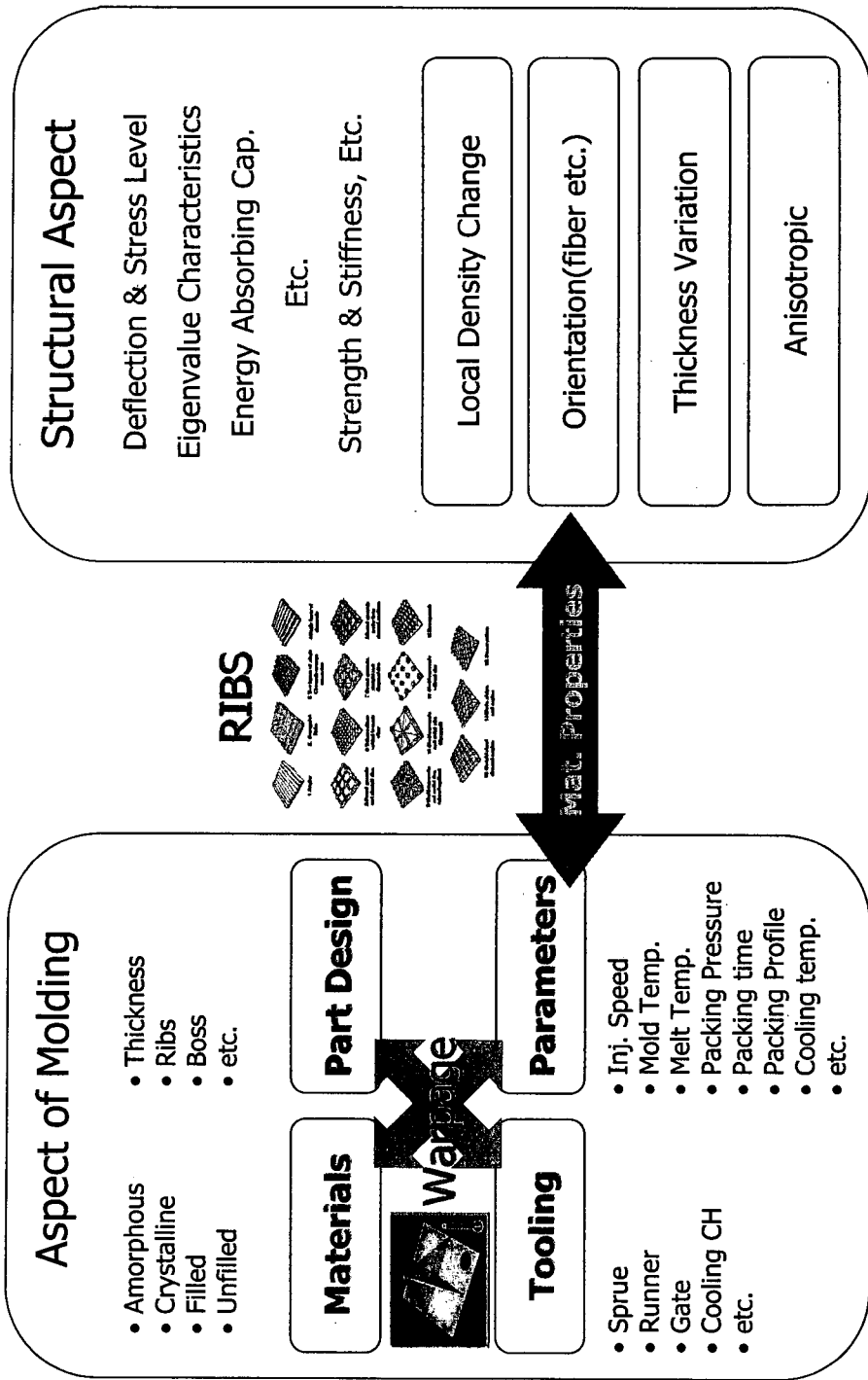
Weld Lines

Flow balance

Racetracking

Warpage







4 Single layer of channels

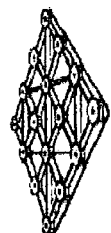
29



8 Round gussets made from channel sections



3 Two layers of single channels arrange crosswise



7 Round gussets, straight and diagonal ribs

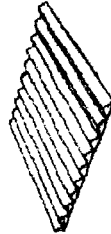


2. Corrugated Plate

83

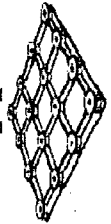


6 Tube sections welded to each other



1 Angles

11



5 Round gussets and straight ribs



9 Starlike gussets and radial ribs (close together)

32



10 Starlike gussets and radial ribs (far apart)

36

30



11 Starlike gussets without ribs

52



13 Straight sheet ribs and angles



15 Weave pattern

30

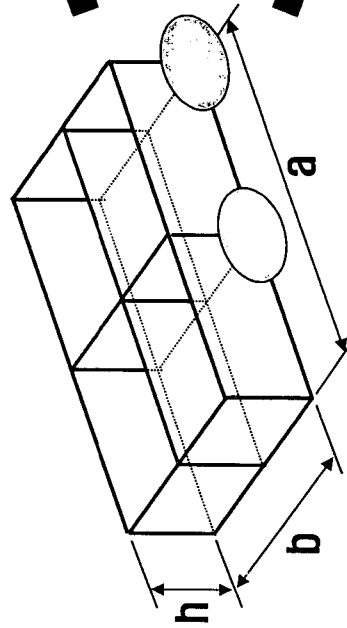


14 Studs, strips, and angles

2. 리스틱 거푸집 패널

일반사출성형모델
(CIM Model)

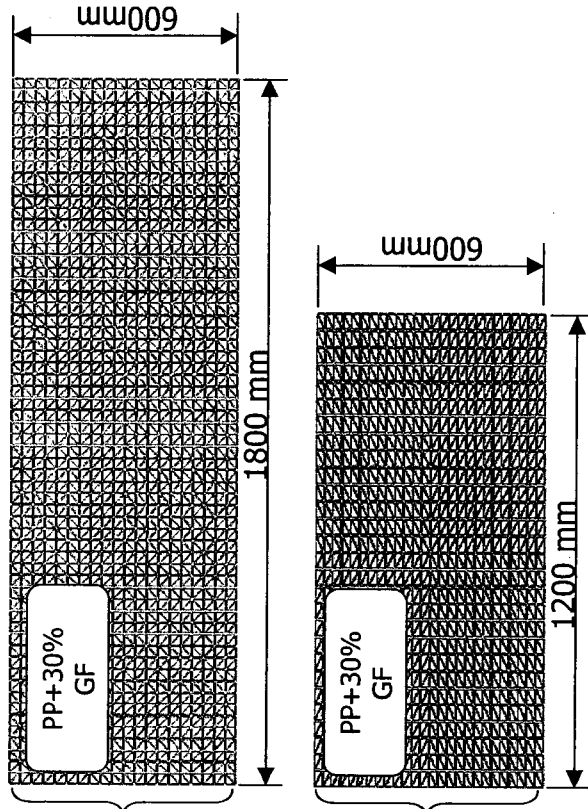
1800x600x4mm, thickness of rib=3mm



<직교리브 평판구조>

일반사출압축성형모델
(ICM Model)

1200x600x4mm, thickness of rib=3mm



3 기본시 유동 이론 개요

Governing Equations

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x}(\rho v_x) + \frac{\partial}{\partial y}(\rho v_y) = 0 \quad (1)$$

$$\frac{\partial}{\partial z} \left(\eta \frac{\partial v_z}{\partial z} \right) - \frac{\partial p}{\partial x} = 0 \quad (2)$$

$$\frac{\partial}{\partial z} \left(\eta \frac{\partial v_y}{\partial z} \right) - \frac{\partial p}{\partial y} = 0 \quad (3)$$

$$\rho C_p(T) \left(\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} \right) = \frac{\partial}{\partial z} \left(\kappa(T) \frac{\partial T}{\partial z} \right) + \eta \dot{\gamma}^2 \quad (4)$$

$$\frac{\partial}{\partial x} \left(S \frac{\partial p}{\partial x} \right) + \frac{\partial}{\partial y} \left(S \frac{\partial p}{\partial y} \right) = G \frac{\partial p}{\partial t} + F \quad (5)$$

$$S = \int \int \rho \int \frac{z}{\eta} dz d\tilde{z}$$

$$G = \int \left(\frac{\partial \rho_l}{\partial p} \right)_T dz + \int \left(\frac{\partial \rho_s}{\partial p} \right)_T dz \quad (6)$$

$$F = \int \left(\frac{\partial \rho_l}{\partial T} \right)_p \frac{\partial T}{\partial t} dz + \int \left(\frac{\partial \rho_s}{\partial T} \right)_p \frac{\partial T}{\partial t} dz \quad (7)$$

$$+ (\rho_l - \rho_s)_{z=0} \frac{\partial \delta}{\partial t}$$

Cross-WLF Viscosity Model

$$\eta(\dot{\gamma}, T, P) = \frac{\eta_0(T, P)}{1 + \left(\frac{\eta_0 \dot{\gamma}}{\tau^*} \right)^{(1-n)}} \quad (8)$$

$$\eta_0 = \begin{cases} D_1 \exp \left[\frac{-A_1(T-T^*)}{A_2 + (T-T^*)} \right] & T > T^* \\ \infty & T \leq T^* \end{cases} \quad (9)$$

$$T^* = D_2 + D_3 P, \quad A_2 = \tilde{A}_2 + D_3 P$$

$n, \tau^*, D_1, D_2, D_3, A_1, \tilde{A}_2$: data fitted coefficients

Tait Formula (PVT)

$$v(P, T) = \begin{cases} (a_{0s} + a_{1s}(T - T_g))(1 - 0.0894 \ln(1 - \frac{P}{B_s})) & (T \leq T_g) \\ (a_{0m} + a_{1m}(T - T_g))(1 - 0.0894 \ln(1 - \frac{P}{B_m})) & (T > T_g) \end{cases} \quad (10)$$

$$T_g = T_{g0} + B_2 P$$

$$B_m = B_{0m} e^{-B_m T}$$

$$B_s = B_{0s} e^{-B_s T} \quad (11)$$

$$C_p(T) = C_1 + C_2 T + C_3 \tanh(C_4 T)$$

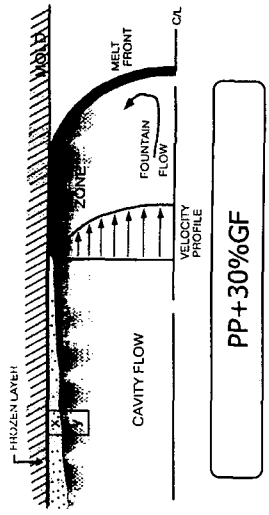
$$\bar{T} = T - C_5$$

C_1, C_2, C_3, C_4, C_5 : Specific Heat Parameters

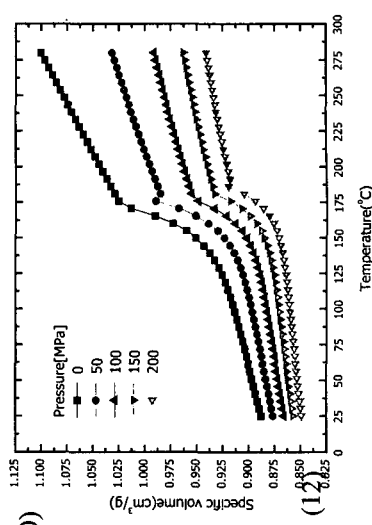
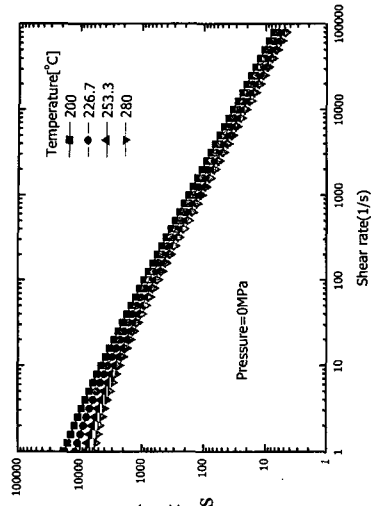
Korea Institute of Industrial Technology

Next

KI EC

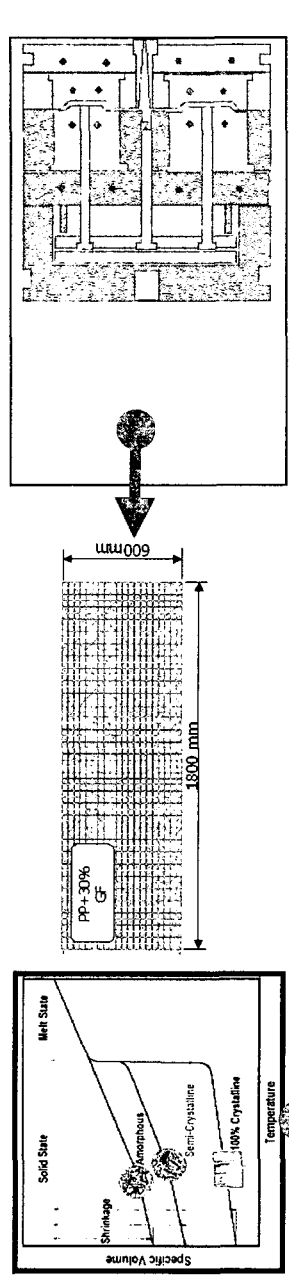


PP+30%GF

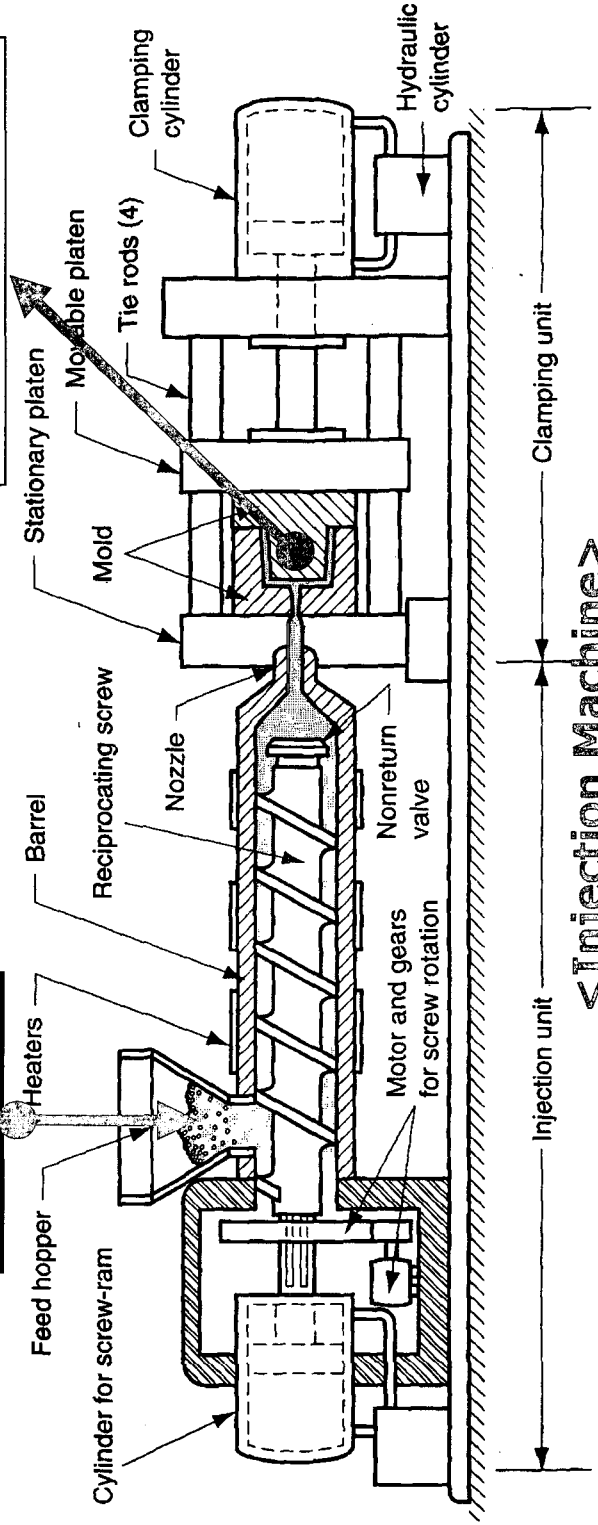


4. 사출성형

Mold & Design



Polymer



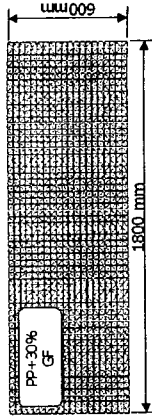
<Injection Machine>

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4. 시공성 평가

- 고분자 수지(Material) : PP+30%GF
- 제품설계(Part Design) : CIM, ICM
- Tooling
- Processing Parameter

Design of Delivery System



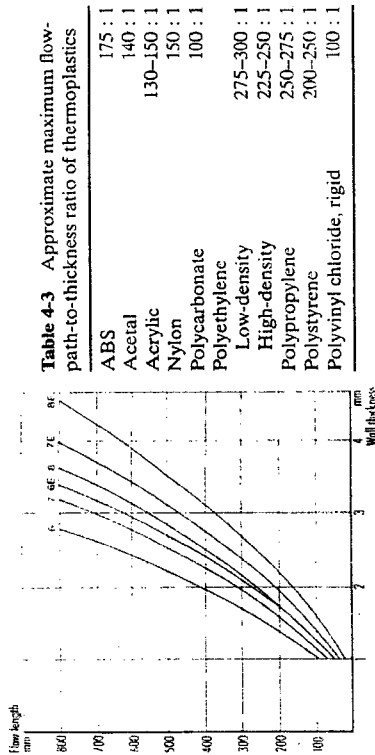
$$D = (w^{1/2} * L^{1/4}) / 3.7$$

$$d_{main} = d_{branch} * N^{1/3}$$

where D = runner diameter (mm)

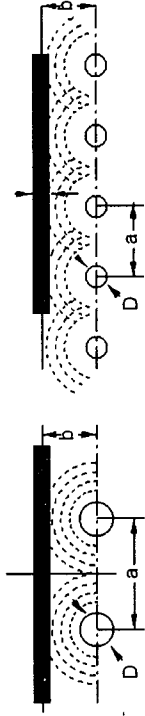
W = part weight (g)

L = runner length (mm)



Relationship between wall thickness and flow length for a number of PMMA molding resins (Degussa Corporation)
 (There are two series of grades: Standard grades 6, 7 and 8, and E-grades with higher molecular weight)

Design of Cooling Channel



	(a) Non-Uniform Heat Removal	(b) Largely Uniform Heat Removal
Design rules:	1. Part thickness W <2mm <4mm <6mm	1. Part thickness W Channel diameter D 8~10mm 10~12mm 12~15mm
	2. Spacing b = 2~3xChannel diameter D	
	3. Spacing a = max3xChannel diameter D	

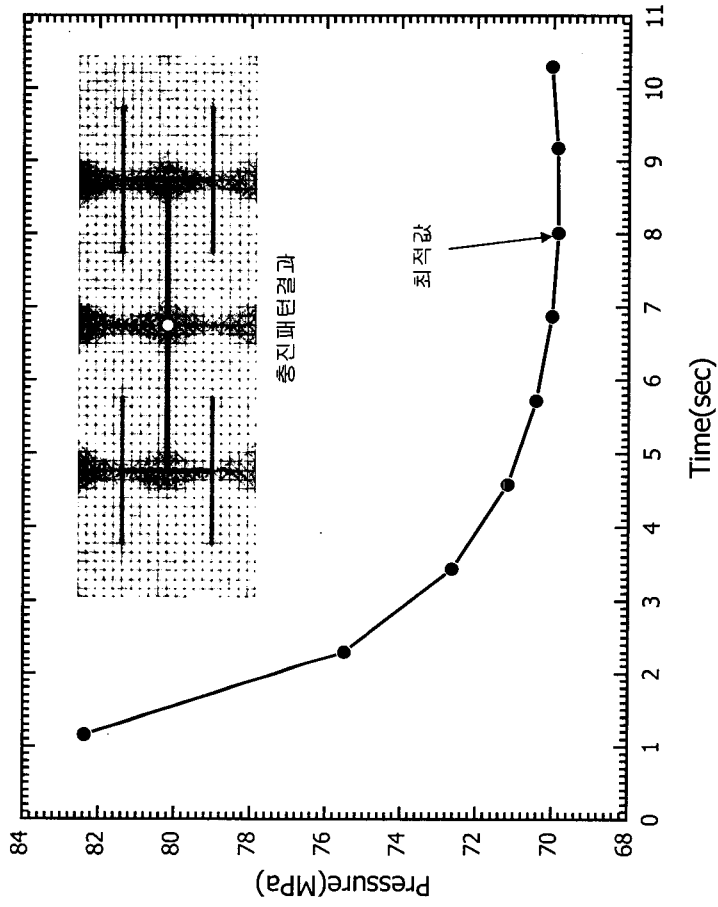
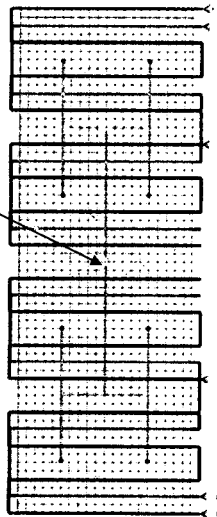
Manufacturing of the Injection Molding



Recommended processing parameters & operating conditions

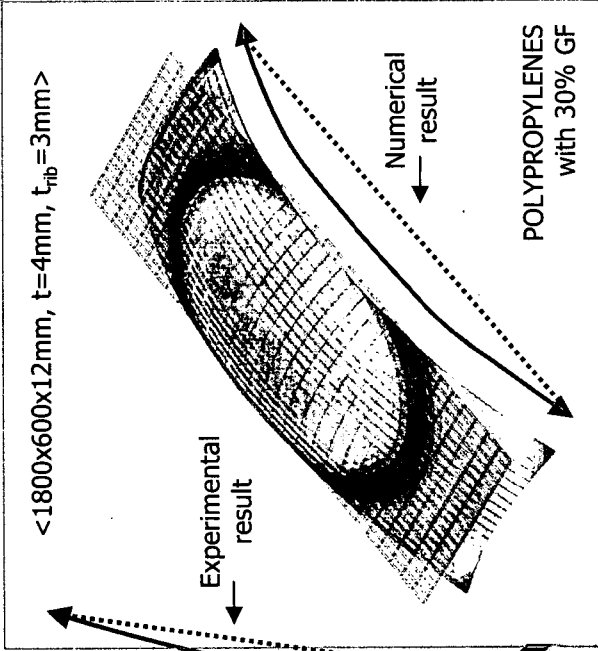
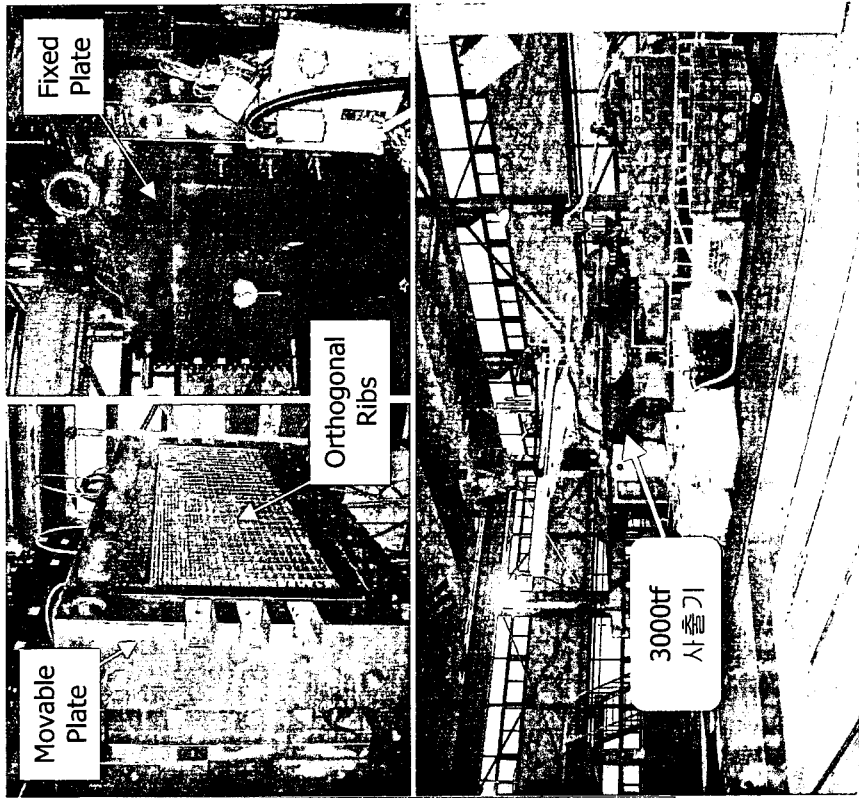
Recommended mold temperature range(°C)	20-80
Recommended melt temperature range(°C)	200-280
Absolute max melt temp(°C)	320
Ejecting temperature(°C)	93

Injection node



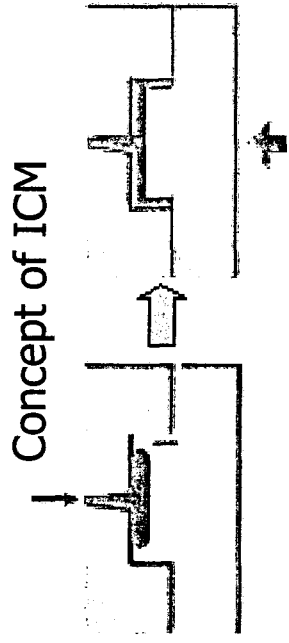
《사출시간의 최적화 결과》

4. 시뮬레이션(해석)

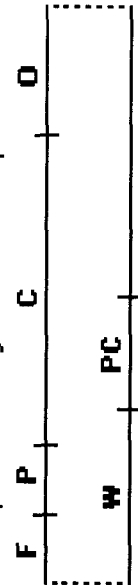


<사출성형해석결과와 실험 결과의 비교>

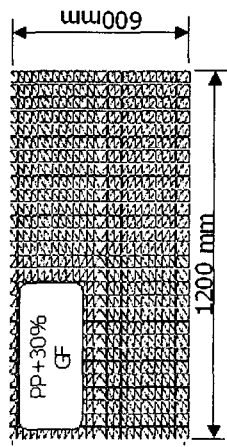
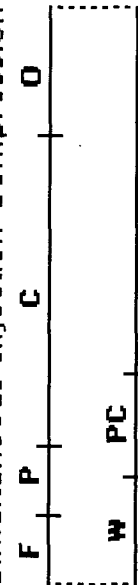
5. 사출압축 성형



Sequential Injection Compression



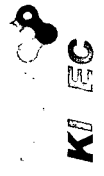
Simultaneous Injection Compression



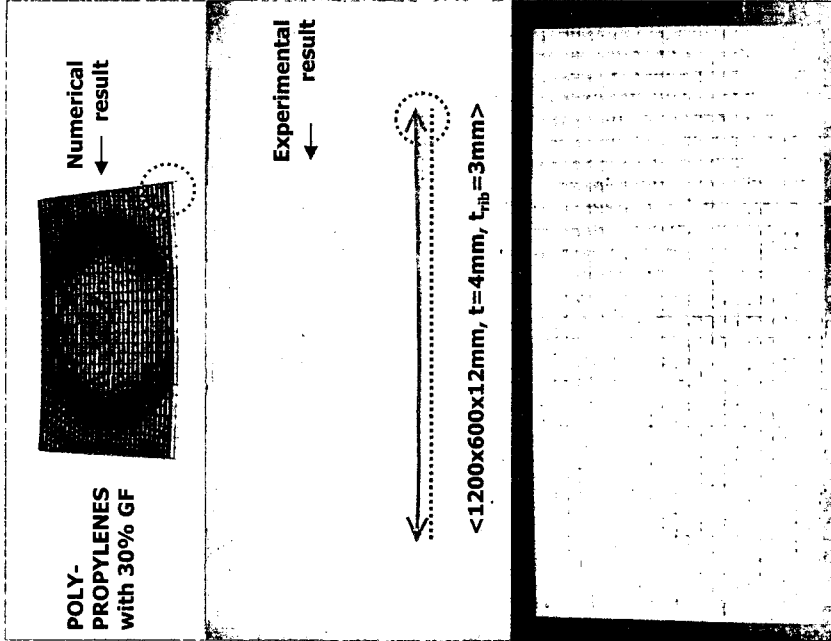
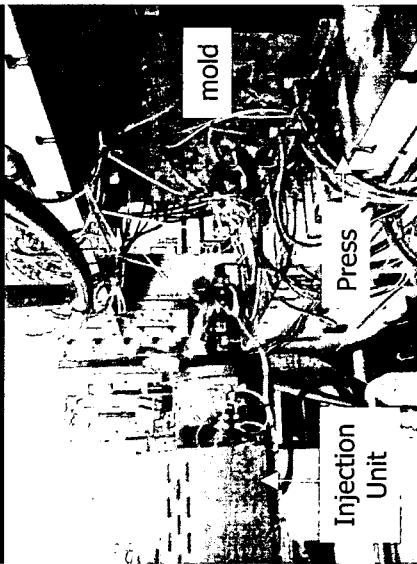
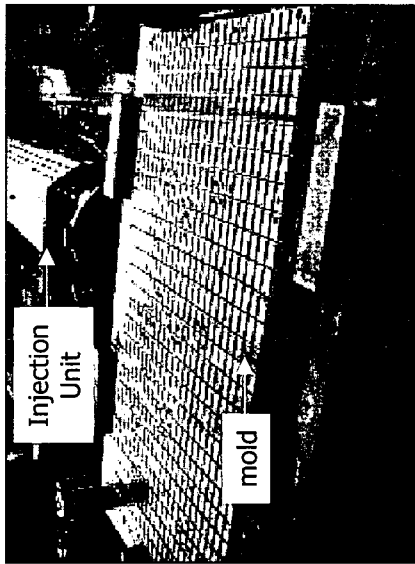
적용된 사출압축 성형조건

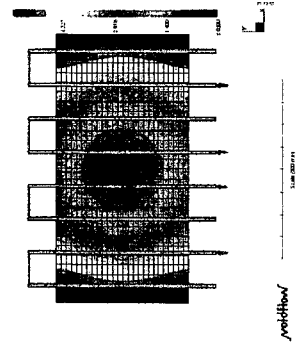
Mold Temperature	50	°C
Melt Temperature	240	°C
Injection Time	5	sec
Cooling Time	150	sec
Coolant	water	
Coolant Temperature	24	°C
Mold Open Distance	6	mm
Compression Delay Time	6	sec
Compression Time	20	sec
Compression Force	150-160	tonf

F: Fill Time, P: Pack Time, C: Cool Time, O: Mold Open Time
 W: Press Waiting Time, PC: Press Compression Time

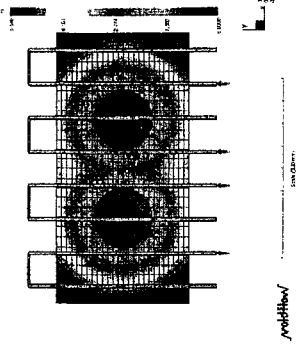


5. 시공인축성형(제외)

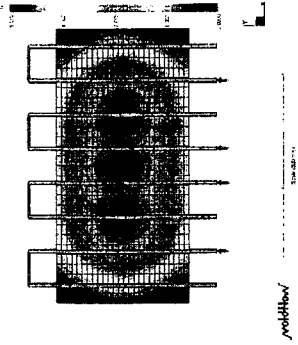




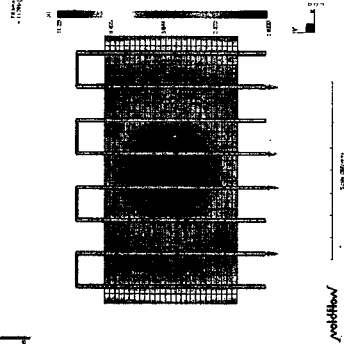
(a) One gate 사출



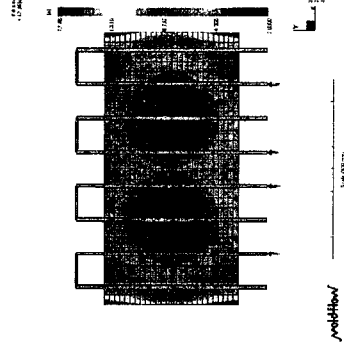
(b) Two gate 사출



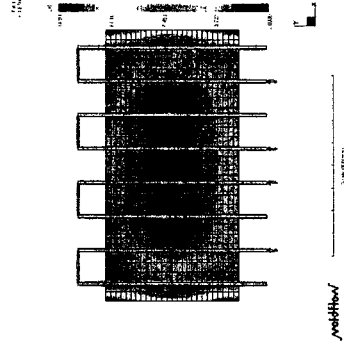
(c) Three gate 사출



(d) One gate 사출/입축



(e) Two gate 사출/입축



(f) Three gate 사출/입축

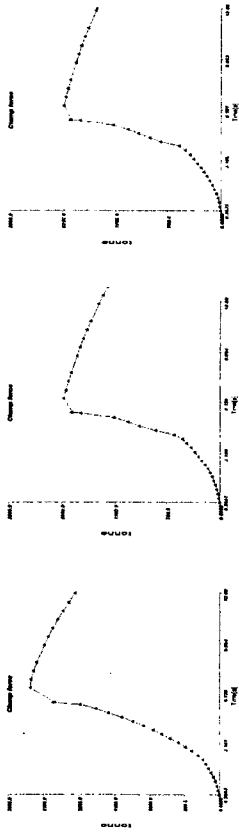
<게이트 변화에

따른 사출성형(상)과

사출압축 성형(하)의

충진패턴비교>

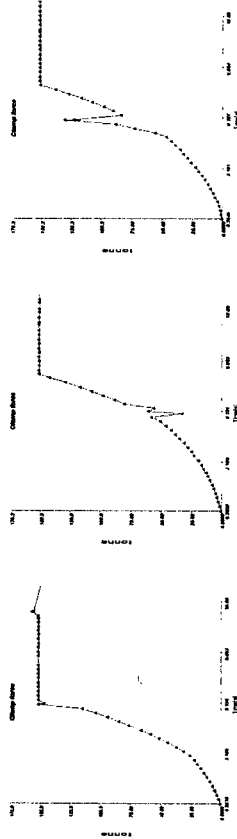
* 냉잉모델(ICM)



(a) One gate 사출

(b) Two gate 사출

(c) Three gate 사출



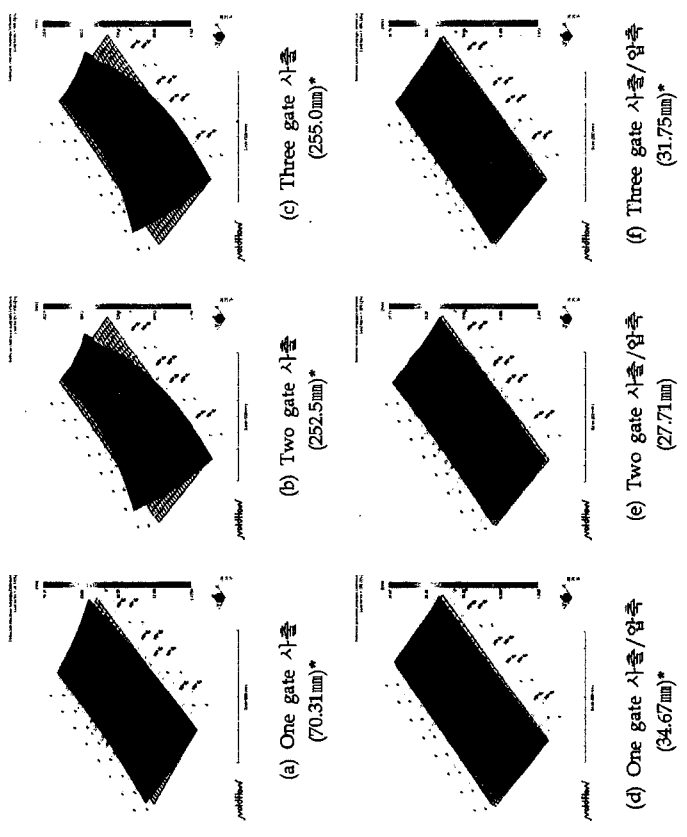
(d) One gate 사출/압축

(e) Two gate 사출/압축

(f) Three gate 사출/압축

<게이트 변화에 따른 사출성형(상)과 사출압축성형(하)의 형체력 비교>
 *동일모델(ICM)

6. 비교 및 고찰(계)



<게이트 변화에 따른 사출성형(상)과 사출압축성형(하)의 횡결과 비교>
 * 동일모델(ICM)



7. 결론 및 향후과제

- 본 연구에서는 초대형 직교 보강 플라스틱의 성형을 위한 일반사출성형과 사출압축성형에 대한 기초 연구를 수행하였다.
- 사출성형에서 힘 최소화 작업을 수행하였으나, 해석 및 실험적으로 만족스러운 결과를 도출하지 못하였다.
- 이러한 원인에는 제품의 초대형성으로 인한 다수개의 게이트 필요에 따른 용융 섬유 보강 수지의 성형시 배향성 효과에 기인한 것으로 판단된다.
- 한편 사출압축성형을 수행한 결과 사출성형대비 약 5%정도의 낮은 형체력으로도 모델의 최대길이 대비 약 1.5%의 양호한 변형(휨)결과를 얻을 수 있었다.
- 하지만 양산제품으로 발전시키기 위해서는 좀더 조직적인 성형조건 최적화를 수행해야 된다고 사료된다.

