# 전기자동차의 다중충전 및 V2G 응용을 위한 새로운 통합 배터리 충전기 구조

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## A Novel Integrated Battery Charger Structure for Multiple Charge and V2G application for Electric Vehicles

#### ABSTRACT

This paper has introduces a novel Integrated On-board Charger (IOBC) to reduce the size, weight and cost of power conversion stages in Electric Vehicles (EVs). The IOBC is composed of an OBC and a low voltage dc-dc converter (LDC). The IOBC includes a bidirectional ac-dc converter and a bidirectional full-bridge converter with an active clamp circuit. The LDC converter is a hybrid topology combining an active clamped full-bridge converter and a forward converter derived from the Weinburg converter topology. Unlike conventional OBC, the proposed IOBC is compact and the LDC converter of it can achieve a higher efficiency. In addition, the LDC converter of the proposed IOBC can achieve high step-down voltage conversion ratio, no circulating current, no reverse recovery current of the rectifier diodes and small ripple current of output inductor on the auxiliary battery. A 1kW hardware of the LDC converter is implemented to verify the performances of the proposed IOBC.

*Index Terms* – Integrated OBC; LDC converter; Hybrid converter, Weinburg converter.

#### 1. Introduction

The energy storage system in Electric vehicles (EVs) and plug-in hybrid electric vehicles (PHEVs) normally consist of two kinds of batteries (low voltage battery, 12V or 24V and high voltage battery, 400V). One is the propulsion battery, which provides high dc voltage for the electric motor. The other is the auxiliary battery, which supplies low dc voltage for electric fields such as lighting, entertainments, signaling circuits, and stereo sound system. To charge for these two batteries, two converters are required: on-board charger (OBC) charging the propulsion battery and LDC converter charging the auxiliary battery. In current dc-dc converters system on EVs or PHEVs, these two converters exists separately, thereby increasing the size and the cost of power conversion system.

IOBC structure has been introduced recently and it combines an OBC and an LDC converter to reduce the size, weight, cost and the rating of the devices. An IOBC can carry out three functions: 1) Charge from grid-to-vehicle (G2V); 2) Discharge from vehicle-to-gird (V2G); 3) Propulsion-to-auxiliary (P2A) as shown in Fig 1. One problem of the integrated OBC converter is that the LDC converter integrated in OBC ca hardly show the as good performance as a separated one. In case of the one in [2], the lower efficiency is attributed to the high conduction loss. The conduction loss is caused by the two stage power conversion. In [3], an IOBC converter was presented based on Voltage/Current-Fed Full-bridge structure. The circulating current can be minimized and soft-switching can be guaranteed for a wide range of load. Based on experimental results, the converter in [3] exhibits a simpler structure and a higher efficiency compared to the converter in [2]. Nevertheless, when the power is delivered from propulsion battery to auxiliary battery, it works like a current-fed converter with an input inductor. This inductor leads to an increase in voltage of transformer, therefore, a high stepdown turns-ratio is required. In additions, rectifier diodes suffer from reverse recovery current which results in a lower performance in high current application.

In this paper a novel IOBC is proposed as shown in Fig. 1. In the proposed topology a novel LDC converter is proposed to solve the problem of high step-down turns-ratio of the transformer in [3]. The proposed LDC converter is a hybrid converter between a PSFB converter and a forward converter. The inductor  $L_{o1}$  is used to deliver the energy during the freewheeling interval of the PSFB converter, as shown in Fig. 2. The full ZVS operation of secondary switches can be achieved by the magnetizing current of the transformer and ZCS of leading leg can be obtained all over the operating condition. The circulating current and reverse recovery current of the diodes are eliminated due to the output capacitor of the forward converter.

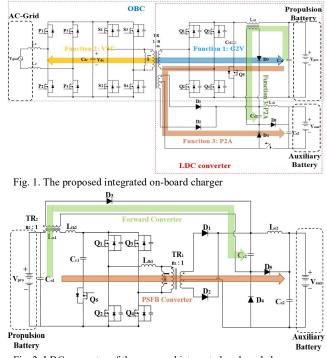


Fig. 2. LDC converter of the proposed integrated on-board charger

2. Operating principle of the LDC converter

Fig. 2 shows circuit diagram of the proposed LDC converter. Mode  $1(t_0 - t_1)$ : The switches  $Q_1$  is turned on with ZVS condition at  $t = t_0$ . The power is transferred to the output through both PSFB converter and forward converter.

Mode  $2(t_1 - t_2)$ : At  $t = t_1$  the switch at  $Q_4$  is turned-off to end the transferring power mode and move on the freewheeling mode.

Mode  $3(t_2 - t_3)$ : The switches  $Q_3$  and  $Q_5$  are turned on with ZVS condition at t=t<sub>2</sub>. The transformer TR<sub>2</sub> is reset by the active clamp switch  $Q_5$ .

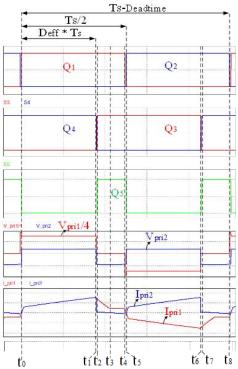


Fig. 3. Key waveforms of the proposed converter

Mode  $4(t_3 - t_4)$ : In the primary side of the PSFB converter, the primary current  $i_{pri1}(t)$  is equal to magnetizing current of the TR<sub>1</sub> because there is no reflected current from the output inductor.

Mode  $5(t_4 - t_8)$ : The operations of the proposed converter in the period from  $t_4$  to  $t_8$  are same as the operations in the period from  $t_0$  to  $t_4$ .

#### 3. Experimental results

The specification of the proposed IOBC can be found in the Table 1. TABLE 1

SPECIFICATION OF THE PROPOSED IOBC		
Stages	Parameters	Value
	DC-link voltage	380 – 420 [V]
Function I (OBC): DC-Link to propulsion battery	Propulsion battery voltage	250-420 [V]
	Rated power	3.3 [kW]
	Efficiency (max/normal)	98.1/97.7 [%]
Function II (OBC): Propulsion battery to DC- Link	DC-link voltage	380-420 [V]
	Propulsion battery voltage	250-420 [V]
	Rated power	3.3 [kW]
	Efficiency (max/normal)	98.1/97.7 [%]
Function III (LDC): Propulsion battery to auxiliary battery	Propulsion battery voltage	250-420 [V]
	Auxiliary battery voltage	23 – 25 [V]
	Rated power	1 [kW]
	Efficiency (max/normal)	96/95.5 [%]

The experimental results of function I and function II are referred from the paper [1].

Fig.4 shows waveform of the lagging switch  $Q_1$  at light load condition of 10% and Fig.5 shows the waveform of the lagging

switch  $Q_1$  at heavy load condition. The ZVS turn-on and nearly ZCS turn-off of the switch  $Q_1$  are proved in both Fig.4 and Fig.5.

The waveform of the leading switch  $Q_3$  is shown in Fig. 6 with ZVS turn-on condition. Fig.7 is the waveform of the primary side transformer  $TR_1$ . It can be seen that there is no circulating current in the freewheeling interval. The waveform of the primary side transformer  $TR_2$  is illustrated in Fig. 8.

In the secondary side of the proposed LDC converter, measured waveform of the diodes  $D_1$  is shown in Fig. 9 with no reverse recovery current. Fig. 10 shows the waveform of the diode  $D_3$  achieving ZCS turn-on and no reverse recovery current.

The efficiency of the proposed LDC converter is shown in Fig. 11 with a wide voltage range of the propulsion battery. The maximum of 96% was achieved in the proposed LDC converter at 500W.

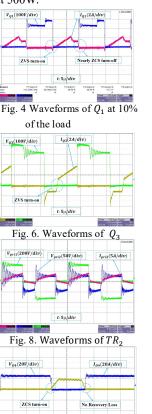
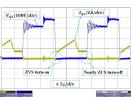
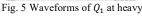
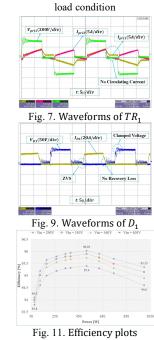


Fig. 10. Waveforms of D<sub>3</sub>







#### 4. Conclusion

This paper has introduced a novel integrated battery charger structure for multiple battery charger to reduce the size, weight and cost of dc-dc converters in EVs. The operating principle of the proposed IOBC has been describe d and its superior performance has been proved by the experimental results. The LDC converter derived from the Weinburg converter topology help increase the voltage step-down conversion ratio and achieve the high efficiency. It is expected that the proposed topology will contribute to the reduction in volume, weight and cost of the power conversion system in electric vehicle system.

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