# **Effect of Cooling Rate on the Hydride Reorientation of Non-irradiated Zircaloy-4 Cladding Tube : 0.5**ଇ**/min vs. 0.5**ଇ**/hr**

DaeHo Kim\*, JongDae Hong, Jegeon Bang, Iksung Lim, EuiJung Kim, and DongHak Kook Korea Atomic Energy Research Institute, 111, Daedeok-daero 989beon-gil, Yuseong-gu, Daejeon, Republic of Korea \*kdh@kaeri.re.kr

# **1. Introduction**

In a dry storage environment, the spent fuel will have a long period of cooling time at high temperatures. At this time, the dissolved circumferential hydride is slowly precipitated from the radial hydride, which makes it more brittle and thus degrading the integrity of the cladding tube. The hydride reorientation occurs by internal rod pressure of the fission gas in cladding tube, and the hoop stress is applied to the outer diameter of the cladding, causing hydrogen to flow in a radial direction.[1]

The effects of cooling rate of hydride reorientation, which could occur during long-term dry storage process in the spent fuel cladding, were evaluated.

### **2. Experiment**

#### *2.1 Hydride Reorientation Test Method*

Using a 400 ppm and 600 ppm of the nonirradiated Zircaloy-4 cladding tube, the hydride reorientation test(HRT) from  $400^{\circ}$  of maximum temperature to  $100^{\circ}$  on decreasing 0.5 $^{\circ}$ C/min and  $0.5^{\circ}$ C/hr were performed at hoop stress 90 MPa respectively. Table 1 and 2 is HRT temperature program of  $0.5^{\circ}$ C/min and  $0.5^{\circ}$ C/hr. And the Fig. 1 is test profiles of temperature and hoop stress.

Table 1. HRT temperature program of short-term [2]

$0.5\degree$ /min Cooling Rate HRT Program								
Segment	Target	Heating(Cooling)	Step Time					
	Temperature	Rate						
	420 $\degree$ C	$+5$ °C/min	$1.20$ hr.min					
2	420 $\degree$ C	Holding	$1.00$ hr.min					
2	$100 \, \mathrm{C}$	$-0.5$ °C/min	10.40 hr.min					
	RT		End					

Table 2. HRT temperature program of long-term [3] 0.5ଇ/hr Cooling Rate HRT Program





Fig. 1. HRT profiles of temperature and hoop stress.

#### *2.2 Specimens and Test Condition*

The test specimen of non-irradiated Zircaloy-4(cold-worked, stress-relief annealed, CWSRA) cladding were 400 ppm and 600 ppm of the treated homogenization hydrogen respectively, using the injection chamber of the volume of a mass system. And each specimen length is 150 mm used fitting at top and bottom. Table 3 lists the specimen and test conditions.

Table 3. Specimen and Test Condition

Specimen				Condition	
Material Length (mm)		Hydrogen Concentration (ppm)	Diameter (mm)	Hoop Stress (MPa)	<b>IRP</b> (MPa)
$Zry-4$	150	400 600	9.5	90	11.536

# **3. Test Results**

After hydride reorientation test of non-irradiated Zircaloy-4 cladding tube, the offset strain was assessed from ring compression test at room temperature,  $100^{\circ}$ C and  $300^{\circ}$ C respectively. And the specimens were reviewed micro-structure of hydride morphology.

#### *3.1 Morphology after HRT*

Fig. 2 is a micro-structure of 400ppm and 600ppm specimen after HRT. Through the visualized review, it is difficult to observe the change in radial hydride.



Fig. 2. Morphology after HRT.

### *3.2 RCT Results at RT*

Table 4 and Fig. 3&4 are ring compression test results at room temperature. At result of offset strain, the 600wppm specimen of long-term cooling speed was assessed the brittle by radial hydride.

Table 4. Results of RCT and Offset Strain

RCT at RT	Hydrogen		Diameter Length		Offset	Offset
	Concentration	(mm)	(mm)	Load	Dis	Strain
	(ppm)			(N)	(mm)	$\binom{0}{0}$
Non-	400	9.50	10.01	907.9	2.53	26.65
<b>HRT</b>	600	9.50	10.00		867.2 2.025	21.32
Short-	400	9.51		925.4	2.51	26.40
term	600	9.50		694.4	0.50	5.26
Long-	400	9.51	9.18	744.9	1.70	17.88
term	600	9.50		655.8	0.23	2.42



Fig. 3. Results of 400 ppm RCT at RT.



Fig. 4. Results of 600 ppm RCT at RT.

Using a 400 ppm and 600 ppm non-irradiated Zircaloy-4 cladding tube, the hydride reorientation test (HRT) from  $400^{\circ}$  of maximum temperature to  $100^{\circ}$  on decreasing  $0.5^{\circ}$  /min and  $0.5^{\circ}$  /hr respectively were performed at hoop stress 90 MPa. The test results of offset strain of the 400 ppm specimen at the short-term cooling rate of  $0.5^{\circ}$ C/min were 26.65%, 26.4% and 17.88% respectively. And the results of offset strain of the 600 ppm specimen at the long-term cooling speed of 0.5 $\degree$ C/hr were 21.32%, 5.264% and 2.42% respectively. In order to assess the effect of the cooling speed on the hydride reorientation, a repetition test is required in various conditions.

## **ACKNOWLEDGEMENT**

This work was supported by the Korea Institute of Energy Technology Evaluation and Planning (KETEP) granted financial resource from the Ministry of Trade, Industry and Energy, Republic of Korea (No. 2014171020166A).

# **REFERENCES**

- [1] Y.J. Kim, "Evaluation of hoop stress on the hydride reorientation and mechanical properties", Proc. of the KRS 2014 Spring Conference, May 8, 2014, Pyung Chang.
- [2] Billone. M.C., "Used Fuel Disposition Campaign, Phase I, Ring Compression Testing of High-Burnup Cladding", ANL-13/05, FCRD-USED02012-000039, 2011.
- [3] Aomi. M, etc. , "Evaluation of Hydride Reorientation Behavior and Mechanical Properties for High-Burnup Fuel-Cladding Tubes in Interim Dry Storage", Journal of ASTM International, Vol. 5, No. 9 2008.