

Thermodynamic Assessment of the $\text{ZrO}_2\text{-TiO}_2$ System

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A thermodynamic assessment for the $\text{ZrO}_2\text{-TiO}_2$ system has been conducted. An optimal thermodynamic data set for this system is evaluated by the CALPHAD(CALculation of PHASE Diagram) method applied to experimental phase diagram and thermodynamic data. The liquid is described by ionic liquid model with two sublattices. The solubilities of the solid solution phases, tetragonal ZrO_2 and TiO_2 (rutile), were described by subregular substitutional model with one sublattice. Two compounds, ZrTiO_4 and ZrTi_2O_6 , are modeled as stoichiometric compounds.

Key words: Thermodynamic assessment, $\text{ZrO}_2\text{-TiO}_2$ phase diagram, CALPHAD, Ionic liquid model

I. Introduction

PZT or modified PZT solid solutions are of interest for many years for their technological applications, which result from their piezoelectric, ferroelectric, and pyroelectric properties.¹⁻³ Nevertheless, attentions were paid mainly to physical properties, kinetics, and device characterizations but a few to phase equilibria and thermodynamic considerations. The quasibinary system $\text{ZrO}_2\text{-TiO}_2$ along with two other quasibinaries PbO-TiO_2 and PbO-ZrO_2 systems are the edges of the quasiternary system $\text{PbO-ZrO}_2\text{-TiO}_2$ system including the technically important PZT solid solution. Also zirconium titanate solid solutions are of interest for their useful dielectric properties in the microwave frequency regime.⁴ Phase diagrams and phase relations of this system have been published by several authors.⁵⁻¹⁴ There is, however, no general agreement among the proposed phase diagrams. This is associated with the sluggish kinetics at relatively low temperatures, the formation of metastable phases, the difficulties in conducting experiments at high temperatures, etc. Major discrepancies were concerned with the existence of intermediated compound, the range of homogeneity of the compound and solid solutions. The determination of the phase relations and thermodynamic properties in zirconia systems can be achieved with relatively a few experiments by means of the CALPHAD method.¹⁵ The application of this method to binary systems can be used to check for internal consistency between thermodynamic and phase diagram data and to provide opti-

mized thermodynamic functions. The calculated ternary phase diagrams and thermodynamic quantities based on the thermodynamic descriptions of the binary diagrams make it possible to design experiments most efficiently. The same is true of going from a ternary to a quaternary system and so on.

The purpose of the present study is to obtain a self-consistent set of parameters for thermodynamic modeling of the $\text{ZrO}_2\text{-TiO}_2$ system allowing evaluation of phase diagrams and relevant thermodynamic data.

II. Experimental Data

ZrO_2 exhibits three polymorphic modifications, which are monoclinic, tetragonal, and cubic forms. For the convenience, they are denoted as ZrO_{2_m} , ZrO_{2_t} , ZrO_{2_c} , respectively. The solid solution based on ZrO_{2_t} is designated as Zss. It is adopted that the monoclinic ZrO_2 transforms to the tetragonal at 1478 K and then the tetragonal to the cubic at 2626 K, which agrees reasonably with the data from Ref. 12 and 13 within experimental errors. TiO_2 exhibits three polymorphic forms, anatase, brookite, and rutile, of which the first two are believed to be metastable with respect to rutile.¹⁶ The solid solution based on TiO_2 is designated as Tss.

It is known that there are several invariant equilibria such as eutectic, eutectoid, peritectic, and peritectoid reaction, two intermediate compounds(ZrTiO_4 , ZrTi_2O_6), and solid solutions of end-members and compounds in the $\text{ZrO}_2\text{-TiO}_2$ system. Some earlier studies of this system have indicated the absence of any compounds in the system and the presence of partial solid solutions.^{5,6} Other previous studies

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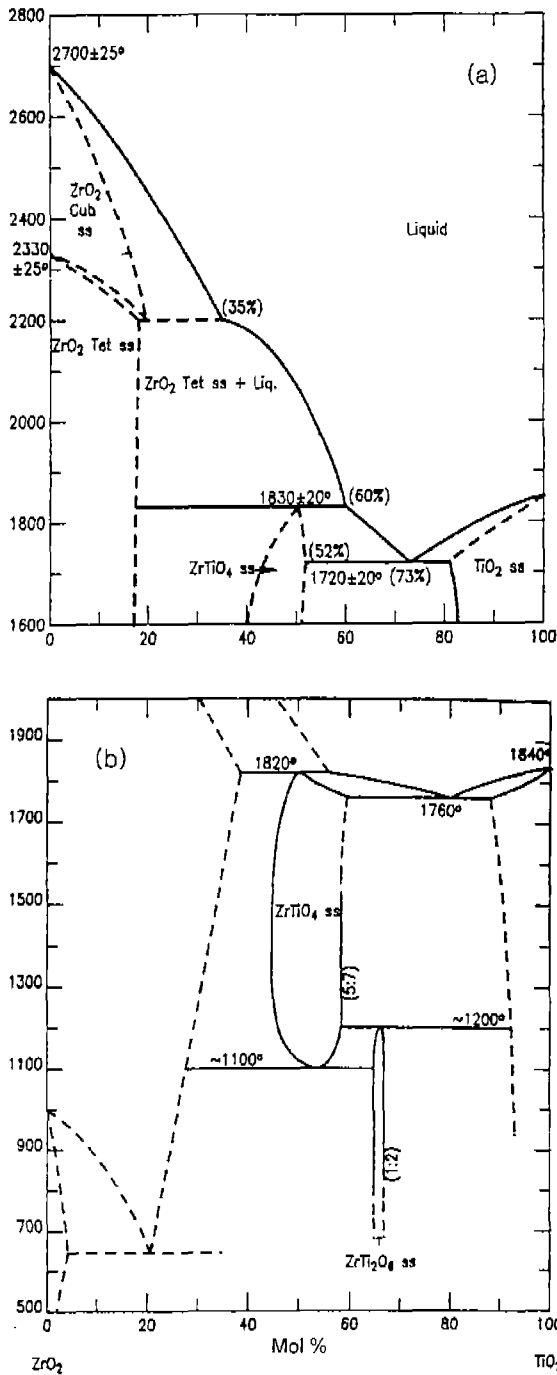


Fig. 1. Phase diagrams of the ZrO_2 - TiO_2 system proposed by A. V. Shevchenko *et al.* (a) and A. E. McHale *et al.* (b).

have proposed the phase diagram including intermediate compound of formula $ZrTiO_4$.⁷⁻¹³ A. E. McHale and R. S. Roth¹⁴ have proposed low temperature phase relations which included new compound $ZrTi_2O_6$ stable below about 1473 K as well as $ZrTiO_4$ stable above about 1373 K. Although investigators agree on solid solution of the end-members and intermediate compound with solid solution, the details of the equilibria are in doubt. Fig. 1 shows some phase diagrams proposed experimentally.

III. Thermodynamic Models

The solution phases including tetragonal ZrO_2 and TiO_2 solid solutions are described by substitutional solution model

$$G_m = x_1 {}^0G_1 + x_2 {}^0G_2 + RT(x_1 \ln x_1 + x_2 \ln x_2) + {}^E G_m \quad (1)$$

where the parameters 0G_i represent the lattice stabilities of pure components i and are given relative to the enthalpy of selected reference state of pure element at 298.15 K. the excess Gibbs free energy is described by Redlich-Kister polynomial formula.

$${}^E G_m = x_1 x_2 \sum_{i=1}^n {}^i L (x_1 - x_2)^i \quad (2)$$

in which the interaction parameter ${}^i L$ may be also temperature-dependent.

The liquid phase is described by ionic liquid model¹⁷ with two sublattices. The liquid can be represented by the formula $(Zr^{+4}, Ti^{+4})_p(O^{-2}, O, Va)_q$, where Va represent hypothetical vacancy and P and Q are the number of sites on the sublattices and vary with composition in order to maintain electroneutrality. The values of P and Q are calculated from the following equations.

$$P = 2y_{O^{-2}} + Qy_{Va}$$

$$Q = 4y_{Zr^{+4}} + 4y_{Ti^{+4}} \quad (3)$$

where y denotes the site fraction of a constituent. P and Q are simply the average charge on the opposite sublattice. The hypothetical vacancies have an induced negative charge equal to Q .

$$\begin{aligned} G_m^l = & y_{Zr^{+4}}y_{O^{-2}} {}^0G_{Zr^{+4}O^{-2}}^l + y_{Ti^{+4}}y_{O^{-2}} {}^0G_{Ti^{+4}O^{-2}}^l + \\ & Qy_{Va}(y_{Zr^{+4}} {}^0G_{Zr^{+4}Va}^l + y_{Ti^{+4}} {}^0G_{Ti^{+4}Va}^l) \\ & + RT\{P(y_{Zr^{+4}} \ln y_{Zr^{+4}} + y_{Ti^{+4}} \ln y_{Ti^{+4}}) \\ & + Q(y_{O^{-2}} \ln y_{O^{-2}} + y_{Va} \ln y_{Va})\} + {}^E G_m^l \end{aligned} \quad (4)$$

where the excess Gibbs energy, ${}^E G_m^l$, is given by

$$\begin{aligned} {}^E G_m^l = & y_{Zr^{+4}}y_{Ti^{+4}}y_{O^{-2}}L_{Zr^{+4}, Ti^{+4}; O^{-2}}^l \\ & + y_{Zr^{+4}}y_{O^{-2}}y_{Va}L_{Zr^{+4}; O^{-2}, Va}^l \\ & + y_{Ti^{+4}}y_{O^{-2}}y_{Va}L_{Ti^{+4}; O^{-2}, Va}^l \\ & + Qy_{Zr^{+4}}y_{Ti^{+4}}y_{Va}L_{Zr^{+4}, i^{+4}; Va}^l \end{aligned} \quad (5)$$

A colon is used to separate constituents in different sublattice whereas a comma constituents in the same sublattice. The parameter L represents the interaction energy between constituents in the sublattice and can be described as follows.

Table 1. Thermodynamic Description of the ZrO₂-TiO₂ system(in J/mol)*** Ionic-liquid**

$${}^0G_{\text{Ti}^{+2},\text{O}^{-2}}^{\text{l}} = 2GTIO2 + 178003 - 62.4769T$$

$${}^0G_{\text{Zr}^{+4},\text{O}^{-2}}^{\text{l}} = -1931250.3 + 272.26T + 2GZRLIQ + 4GHSEROO$$

$${}^0G_{\text{Zr}^{+4},\text{O}}^{\text{l}} = 2648.0 + 31.44T + GHSEROO$$

$${}^0G_{\text{Zr}^{+4},\text{Va}}^{\text{l}} = GZRLIQ$$

$${}^0L_{\text{Zr}^{+4},\text{Ti}^{-4},\text{O}^{-2}}^{\text{l}} = -50000 - 25T$$

$${}^0L_{\text{Zr}^{+4},\text{Ti}^{-2},\text{Va}}^{\text{l}} = 424351.51 - 215.70189T$$

$${}^0L_{\text{Zr}^{+4},\text{Ti}^{-2},\text{Va}}^{\text{l}} = 211955.21 - 77.30708T$$

*** TiO₂ solid solution(Tss)**

$${}^0G_{\text{TiO}_2} = GTIO2 + 22057.5$$

$${}^0G_{\text{ZrO}_2}^{\text{Tss}} = {}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-t}} + 25000$$

$${}^0L_{\text{TiO}_2,\text{ZrO}_2}^{\text{Tss}} = -18600 + 4T$$

*** ZrO₂**

$${}^0G_{\text{Zr},\text{O}_2}^{\text{ZrO}_2\text{-m}} = -1103376.90 + 247.58658T - 0.076129T\ln(T) +$$

$$GHSEZRZ + 2GHSEROO$$

$${}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-c}} = -1014781.7 - 269.4T + 59.015088T\ln(T)$$

$$-0.017726352T^2 + GHSEZRZ + 2GHSEROO$$

*** ZrO₂-t solid solution(Zss)**

$${}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-t}} = -1036480.92 - 261.13659T + 59.015088T\ln(T) -$$

$$17.726352 \cdot 10^{-3}T^2 + GHSEZRZ + 2GHSEROO$$

$${}^0G_{\text{ZrO}_2}^{\text{Zss}} = {}^0G_{\text{TiO}_2} + 35000$$

$${}^0L_{\text{ZrO}_2,\text{TiO}_2}^{\text{Zss}} = -10000 + 15T$$

$${}^1L_{\text{ZrO}_2,\text{TiO}_2}^{\text{Zss}} = 100000$$

*** Intermediate compounds**

$${}^0G_{\text{ZrTiO}_4} = {}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-m}} + {}^0G_{\text{TiO}_4} + 4959 - 12T$$

$${}^0G_{\text{ZrTi}_2\text{O}_6} = {}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-m}} + 2{}^0G_{\text{TiO}_2} - 31260 + 11T$$

GHSEZRZ

$$298.15 < T < 2128.0$$

$$-7827.595 + 125.64905T - 24.1618T\ln(T) -$$

$$4.37791 \cdot 10^{-3}T^2 + 34971T^{-1}$$

$$2128.00 < T < 6000.0$$

$$-26085.921 + 262.724183T - 42.144T\ln(T) - 1342.895 \cdot 10^{28}T^{-9}$$

GHSEROO

$$298.15 < T < 1000.0$$

Table 1. Continued.

$$-3480.87 - 25.503038T - 11.136T\ln(T) -$$

$$0.005098888T^2 + 6.61846 \cdot 10^{-7}T^8 - 38365T^{-1}$$

$$1000.0 < T < 3300.0$$

$$-6568.763 + 12.65988T - 16.8138T\ln(T) - 5.95798E -$$

$$4T^2 + 6.781 \cdot 10^{-9}T^8 + 262905T^{-1}$$

$$3300.0 < T < 6000.0$$

$$-13986.728 + 31.259625T - 18.9536T\ln(T) - 4.25243 \cdot 10^{-4}T^2 +$$

$$1.0721 \cdot 10^{-8}T^8 + 4383200T^{-1}$$

GZRLIQ

$$298.15 < T < 2128.0$$

$$+ 18147.703 - 9.080762T + 1.6275 \cdot 10^{-22}T^7 + GHSEZRZ$$

$$2128.0 < T < 6000.0$$

$$+ 17804.649 - 8.91153T + 1.343 \cdot 10^{31}T^{-9} + GHSEZRZ$$

GTIO2

$$298.15 < T < 700.0$$

$$-966880.638 + 348.553035T - 57.02081T\ln(T) -$$

$$0.020171715T^2 + 3.85969167 \cdot 10^{-6}T^8 + 528343 \cdot T^{-1}$$

$$700.0 < T < 2130.0$$

$$-974253.514 + 461.204893T - 74.51871T\ln(T) -$$

$$0.0013569695T^2 + 2.101665 \cdot 10^{-8}T^3 + 1126927T^{-1}$$

$$2130.0 < T < 4000.0$$

$$-1022606.35 + 679.832804T - 100.416T\ln(T)$$

$${}^0L_{C_1,C_2:A_1} = {}^0L_{C_1,C_2:C_1} + {}^1L_{C_1,C_2:A_1}(y_{C_1} - y_{C_2}) +$$

$${}^2L_{C_1,C_2:A_1}(y_{C_1} - y_{C_2})^2 + \dots \quad (6)$$

where the ⁱL coefficients can depend on temperature and C_i represent cations C_i and A_i anions. ⁰L, ¹L and ²L are so called regular, subregular and subsubregular solution parameters, respectively.

Gibbs free energy of ZrTiO₄ and ZrTi₂O₆, which are treated as stoichiometric compounds are given respectively as follows:

$${}^0G_{\text{ZrTiO}_4} = {}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-m}} + {}^0G_{\text{TiO}_2} + 4959 - 12T \quad (7)$$

$${}^0G_{\text{ZrTi}_2\text{O}_6} = {}^0G_{\text{ZrO}_2}^{\text{ZrO}_2\text{-m}} + 2{}^0G_{\text{TiO}_2} - 31260 + 11T \quad (8)$$

IV. Assessment

The assessment of the model parameters was made by means of Thermo-Calc software and database system.¹⁸ Thermodynamic description of pure elements used in the present work is from the SGTE(Scientific Group Thermo-Data Europe) databank.¹⁹ ZrTiO₄ and ZrTi₂O₆ compounds, which were reported to have the range of homogeneity, are treated as stoichiometric compounds.

The binary description of Zr-O and Ti-O systems was adopted, which has been obtained by authors in the previous work and B.-J. Lee,²⁰ respectively. The accuracies are changed by trial and error until most of the selected experimental information is satisfactorily described. The optimal set of parameters obtained in the current work is given in Table 1.

V. Results and Discussion

The whole ZrO₂-TiO₂ phase diagram calculated from the present set of parameters is given in Fig. 2. The calculated invariant equilibria are compared with the experimental ones in Table 2, which shows fair agreement. The high temperature peritectic reaction, Liquid+ZrO_{2_c}→Zss is a result of the present work. No reliable information about the ZrO₂-rich region above 2500 K has been reported due to the difficulties in conducting experiments at high temperatures. Several authors^{7,12,13} have reported tentatively but so much different phase equilibria about this region. Since the

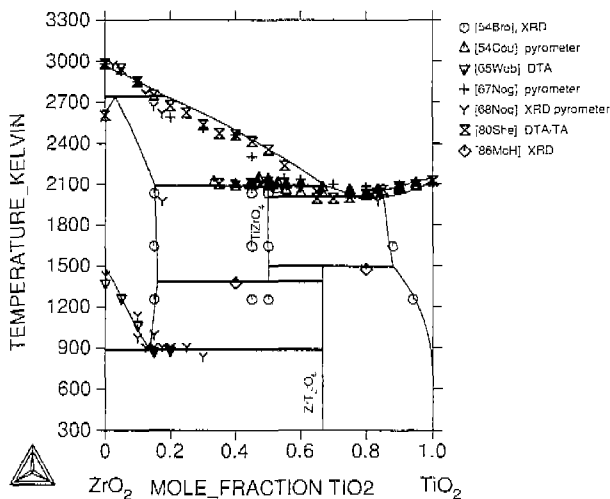


Fig. 2. Calculated phase diagrams of the ZrO₂-TiO₂ system with the experimental phase diagram data. ZrTiO₄ and ZrTi₂O₆ are treated as stoichiometric compounds.

Table 2. Comparison of Calculated and Experimental Invariant Equilibria

Reactions	Experimental	Calculated
Liq.+Zss↔ZrTiO ₄	2093 K ⁹ 2103±20 K ¹⁴	2086.5 K
Liq.↔ZrTiO ₄ +Tss	2033 K ⁹ 1993±20 K ¹⁴	2005.1 K
ZrTiO ₄ +Tss↔ZrTi ₂ O ₆	~1473 K ¹⁵	1497.6 K
ZrTiO ₄ ↔Zss+ZrTi ₂ O ₆	~1373 K ¹⁵	1382.2 K
Zss ZrO _{2_m} +ZrTi ₂ O ₆	~903 K ¹³ 953 K ¹⁵	887.6 K
Liq.+ZrO _{2_c} ↔Zss		2744.3 K

low temperature eutectoid reaction, Zss↔ZrO_{2_m}+ZrTi₂O₆ is also very hard to be established experimentally because of the difficulties in achieving equilibrium at low temperatures and the occurrence of a diffusionless transition between ZrO_{2_t} and ZrO_{2_m}, there have been no agreement among reaction temperatures and compositions previously reported.^{7,12,13} The field of Zss(the boundary between Zss and Zss+ZrTiO₄) calculated in the present work agrees with the results of F. H. Brown *et al.*,⁷ A. Cocco *et al.*,⁹ and T. Noguchi *et al.*¹² but have lower extent than those of L. W. Coughanour *et al.*,⁸ and A. E. McHale *et al.*¹⁴ The field of Tss calculated agree with the results of F. H. Brown *et al.*⁷ The calculated liquidus curves are nearly in agreement with the experimental ones from Ref. 11-13. The range of homogeneity of intermediate compounds, ZrTiO₄ and ZrTi₂O₆, considered as stoichiometric compounds is to be calculated by thermodynamic models.

VI. Summary

The phase diagram and thermodynamic data available for the ZrO₂-TiO₂ system have been considered in the present assessment. An attempt has been made to provide the consistent set of thermodynamic parameters describing the system by coupling CALPHAD method using Thermo-Calc software and database system. The set of thermodynamic functions is for a simplified version of the ZrO₂-TiO₂ phase diagram in which ZrTiO₄ and ZrTi₂O₆ is treated as stoichiometric compounds. Comprehensive comparisons with the experimental data available are made, and it is shown that the set can satisfactorily account for most of the experimental data except for the homogeneity data of ZrTiO₄ and ZrTi₂O₆.

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