

## Change of working length in curved canals by various instrumentation techniques

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### ABSTRACT

To evaluate the change of working length with various instrumentation techniques in curved canals, working length and canal curvature were determined before and after canal instrumentation in buccal or mesial canals of extracted human molars. Stainless steel K-files (MANI®, Matsutani Seisakusho Co. Takanezawa, Japan), nickel-titanium K-files (Naviflex NT™, Brassler, Savannah, USA), ProFile®, and ProTaper™ (Dentsply-Maillefer, Ballaigues, Switzerland) were used to prepare the canals with crown-down technique. In two hand instrumentation groups, coronal flaring was made with Gates Glidden burs. Apical canals were instrumented until apical diameter had attained a size of 30. Positional relation between the tooth apex and the #10 K-file tip was examined by using AutoCAD 2000 (Autodesk Corp., San Rafael, CA, USA) under a stereomicroscope before and after coronal flaring, and after apical instrumentation. Degree of canal curvature was also measured with Schneider's method in radiographs. Data of working length and canal curvature changes were statistically analyzed with one-way ANOVA and Tukey's studentized range test.

Working length and canal curvature were decreased significantly in each step in all instrumentation groups. Coronal flaring using Gates Glidden burs in hand instrument groups and whole canal instrumentation using stainless steel hand K-files caused significantly more working length change than in ProFile instrumentation group ( $p < 0.05$ ).

The result of this study demonstrates that all of the above kinds of instrumentation in curved canals cause reduction of working length and canal curvature at each instrumentation steps, and hand instrumentation causes more working length change than ProFile. (J Kor Acad Cons Dent 31(1):30-35, 2006)

**Key words:** Working length, Curved canal, Hand instrumentation, Rotary instrumentation, ProFile, Canal curvature

- Received 2005.8.23., revised 2005.10.26., accepted 2005.12.5. -

### I . Introduction

The objective of root canal preparation is to clean and shape the root canal system, while maintaining the original configuration. A continuously tapering, conical, funnel-shaped canal with the smallest diameter at the end point and the largest at the orifice has been perceived to be the

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most appropriate for filling with gutta-percha<sup>11</sup>.

In small curved canal, it is difficult to achieve this object. During root canal preparation, aberrations such as apical zipping, canal transportation, ledge, and strip perforation often occur, which inversely influence on the treatment success<sup>11</sup>. Tendency of files to straighten in the canal removes excessive amount of dentin from the inner wall of the curvature at the curve and the outer wall of it at the root end<sup>2,3</sup>. This effect causes straightening the canal and thus may shorten the working length.

Many techniques and various instruments have been developed in an attempt to improve the quality of root canal treatment in curved canals. Anticurvature filing<sup>4</sup>, step-back filing<sup>2</sup>, crown-down pressureless filing<sup>5</sup>, and balance forced technique<sup>6</sup> were introduced. In spite of improvements in instrument design and in various root canal preparation methods, stainless steel hand files still tend to create a number of aberrations in curved canals<sup>2,7</sup>.

During the last decade, various kinds of root canal instruments made of nickel-titanium alloys were developed. Nickel-titanium instruments were found to have 2 to 3 times more elastic flexibility of the stainless steel files in bending and torsion, as well as superior resistance to torsional fracture<sup>8</sup>. Nickel-titanium files were more effective in maintaining the original canal path of curved root canal<sup>7,9-11</sup>. Different kinds of canal instrument and canal preparation technique may exert different effects on working length. If working length is shortened during the course of treatment, overinstrumentation and overfilling may occur. This may cause error of canal shaping and delay healing of periapical lesion.

Therefore, the aim of this study was to evaluate the change of working length with various instrumentation techniques in curved canals.

## II. Materials and Methods

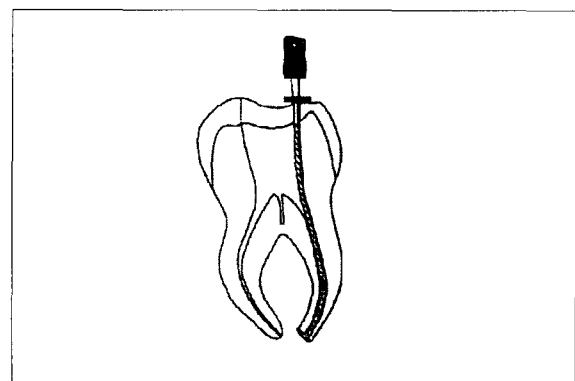
Buccal canals of maxillary molars and mesial canals of mandibular molars were used. Using the technique described by Schneider<sup>12</sup>, canal curva-

ture of root was determined and recorded. Canals having curvature above 20 degrees were selected.

Occlusal surface of teeth was flattened by using diamond point and sandpaper. After access cavity preparation, lingual surface of teeth were embedded in acrylic resin so that the maximum of canal curvature can be seen and root apex was flattened to facilitate reproducible accurate measurements (Figure 1).

Forty specimens were divided into four groups according to the two kinds of hand instruments and two kinds of rotary instruments used: stainless steel hand file (MANI®, Matsutani Seisakusho Co., Takanezawa, Japan), nickel titanium hand file (Naviflex NT™, Brassler, Savannah, USA), ProFile®, and ProTaper™ (Densply-Maillefer, Ballaigues, Switzerland). A #10 K-file was introduced into the canal of each specimen and was placed against a flattened root apex using stereomicroscope. Rubber stop was fixed with a glue and working length was determined. Each canal was instrumented until apical diameter had attained a size of 30. Root canals were irrigated with NaOCl and RC-Prep (Stone Pharmaceuticals, Philadelphia, USA) was used as a lubricant.

In two hand file groups, #2 and #3 Gates Glidden drill were used to flare the coronal third of the canal and crown-down pressureless technique<sup>5</sup> was used. A #30 file was placed into the canal until resistance was first encountered and



**Figure 1.** Occlusal cusp and root apex were flattened to obtain an accurate measurement of working length.

whole procedure was used until apical file size of #30 was obtained.

In ProFile group, Orifice Shaper #3 and #2 were used until resistance was encountered (12 to 15 mm) for coronal flaring. The .06/#25 and .06/#20 files were used serially to the resistance (within 1 to 2 mm of the working length). For apical shaping, .04/#25 and .04/#30 files were used to the working length.

In ProTaper group, SX, S1, and S2 files were used for coronal flaring. S1 was used first and moved apically to 2 mm short of the working length. SX files were then used sequentially until resistance was encountered (4 to 5 mm from the working length), followed by S1 and S2 to the working length for the shaping of the coronal two thirds of the canal. The apical one third was finished by using F1, F2 and F3 sequentially to the working length, with only one pecking motion for each instrument.

Working length change was examined before and after finishing the coronal flaring and after finishing the apical preparation. Positional relation between the tooth apex and the file tip was examined before and after coronal flaring and after apical preparation under a stereomicroscope, and the images were stored in a computer using a CCD camera and micro VIDEO Studio 200 program. The change of file tip position was measured by using AutoCAD 2000 (Autodesk Corp., San Rafael, CA, USA).

Root canal curvature was measured in radiograph with K-file in the canal using Schneider's method<sup>12)</sup> before and after coronal flaring, and after apical preparation.

The data were analysed using one-way ANOVA and Tukey's studentized range test.

### III. Results

Working lengths were decreased significantly in each stage in all instrumentation groups. Coronal flaring using Gates Glidden burs in hand file groups caused significantly more working length change than in ProFile instrumentation group ( $p < 0.05$ ) (Figure 2).

Whole canal instrumentation in stainless steel hand file group caused significantly more working length decrease than in ProFile instrumentation group ( $p < 0.05$ ) (Figure 2).

Canal curvature was decreased in all groups. There was no significant different in the change of canal curvature after coronal flaring among groups.

Apical preparation using either stainless steel hand file or ProTaper caused significantly more decrease of canal curvature than in ProFile ( $p < 0.05$ ).

Whole canal instrumentation in either stainless steel hand file group or ProTaper group caused significantly more decrease of canal curvature than in ProFile instrumentation group ( $p < 0.05$ ) (Figure 3).

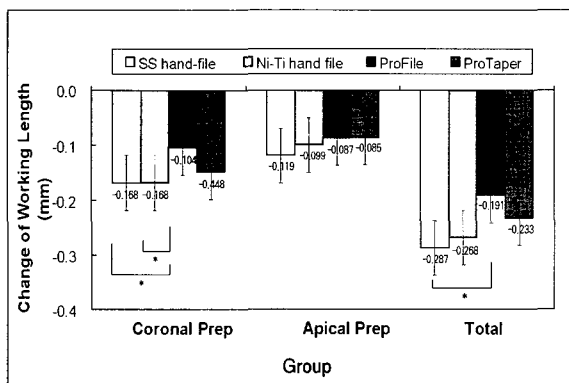


Figure 2. Change of working length by instrumentation (mean  $\pm$  SD). \* Statistically significant ( $p < 0.05$ ).

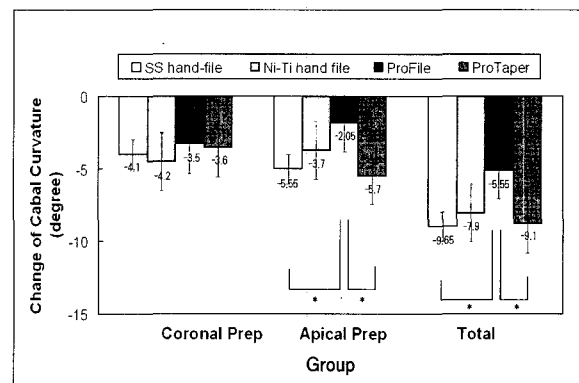


Figure 3. Change of canal curvature by instrumentation (mean  $\pm$  SD). \* Statistically significant ( $p < 0.05$ ).

#### IV. Discussion

In the present study, working length was decreased in all canals, indicating that shortening of working length occurs during the instrumentation in curved canals. A number of studies reported shortening of working length<sup>13-17</sup>. Schroeder *et al.*<sup>16</sup> reported that change of working length by Gates Glidden drill was 0.17 mm. In the present study, change of working length by coronal flaring is similar with the result of Schroeder *et al.*<sup>16</sup>. The finding that ProFiles caused the smallest change in working length are in agreement with those of Thompson and Dummer<sup>18,19</sup>, Bryant *et al.*<sup>20,21</sup>, and Kum *et al.*<sup>22</sup> who evaluated length change associated with the use of nickel-titanium rotary files. According to Thompson and Dummer<sup>18,19</sup>, Bryant *et al.*<sup>20,21</sup>, and Kum *et al.*<sup>22</sup>, nickel-titanium rotary files caused minimal change in canal configuration.

In the present study, change of working length and change of canal curvature were measured. Coronal flaring using Gates Glidden burs in hand instrument groups and whole canal instrumentation in stainless steel hand file group caused significantly more working length change than in ProFile instrumentation group. This result is also similar with the report of Davis *et al.*<sup>17</sup>. Nickel-titanium files were more effective in maintaining the original canal path of curved root canals, so this is reasonable result. Also, change of canal curvature in ProFile group after apical preparation and whole canal instrumentation significantly smaller than in stainless steel hand file group and ProTaper group.

Kim *et al.*<sup>15</sup> reported that decrease of working length and canal curvature occurred during canal preparation using ProFile and greatest change of curvature and working length were observed in above 30 degrees.

In the present study, working length and curvature was decreased in all groups. Significantly smaller decrease in curvature was observed in ProFile group than in stainless steel K-file group and ProTaper group. Since the group of the greatest change of canal curvature showed the greatest

change of working length as well, and the group of the smallest change of canal curvature showed the smallest change of working length as well in the present study, the main cause of the change of working length will be the change of canal curvature. Because of decrease of curvature, working length may be decreased, and also file didn't passed by center of canal and was straightened in canal, this may cause decrease of working length. Therefore, decrease of working length will occur even when decrease of curvature don't observed. In the present study, because canal curvature was determined by measuring curvature of file, change of canal curvature in this study may be different from the exact change of canal curvature and may be greater than that.

In response to the problems with the traditional step-back preparation method, there has been a trend toward the crown-down technique, which involves preparing a canal from the cervical aspect to the apex, rather than the classical approach from the apex to the crown<sup>23</sup>.

The crown-down technique using nickel-titanium files with increased tapers allows easier access to the canal, improves distribution of irrigant and induces less extrusion of debris than other technique<sup>11</sup>.

ProTaper is a Ni-Ti rotary file with high taper and high cutting ability. ProTaper removed significantly more canal material than ProFile, GT file, and Quantec, and cause decrease in canal curvature. ProTaper removed more material from the inner side of canal before the initiation of curve, but in the apical third area, they removed more material from the outer side of canal, which resulted in a decrease in curvature<sup>24</sup>. ProTaper removed more root dentin than GT Rotary, Quantec, and ProFile at danger zone<sup>25</sup>. Therefore, canal preparation using ProTaper may cause greater shortening of working length than other Ni-Ti instruments.

If working length is shortened during the course of treatment, overinstrumentation and overfilling may occur. This may cause error of canal shaping and delay healing of periapical lesion. In the present study, both the coronal flaring and the apical

preparation caused change of working length in each group, and change of working length by coronal flaring was greater than that by apical preparation. Therefore, using the working length measured before root canal preparation may cause overinstrumentation. Hence, if an operator wants to measure working length only once, it will be recommended to do it after coronal flaring rather than before root canal preparation.

The result of the present study demonstrates that working length and canal curvature decrease with all kinds of instrumentation techniques. Therefore, special caution is needed to minimize them and redetermination of working length will be necessary before final instrumentation. Further research is needed to evaluate the change of working length and apical canal shape with various designs of endodontic instruments.

## References

1. Schilder H. Cleaning and shaping the root canal. *Dent Clin North Am* 18:269-296, 1974.
2. Weine FS, Kelly RF, Lio PJ. The effect of preparation procedures on original canal shape and on apical foramen shape. *J Endod* 1:255-262, 1975.
3. Alodeh MH, Doller R, Dummer PN. Shaping of simulated root canals in resin blocks using the step-back technique with K-files manipulated in a simple in/out filing motion. *Int Endod J* 22:107-117, 1989.
4. Abou-Rass M, Frank AL, Glick DH. The anticurvature filing method to prepare the curved root canal. *J Am Dent Assoc* 101:792-794, 1980.
5. Morgan LF and Montgomery S. An evaluation of the crown-down pressureless technique. *J Endod* 10:491-498, 1984.
6. Roane JB, Sabala CL, Duncanson MG. The "balance force" concept for instrumentation of curved canals. *J Endod* 11:203-211, 1985.
7. Esposito PH, Cunningham CJ. A comparison of canal preparation with nickel-titanium and stainless steel instrument. *J Endod* 21:173-176, 1995.
8. Walia H, Brantley WA, Gerstein H. An initial investigation of the bending and torsional properties of nitinol root canal files. *J Endod* 14:346-357, 1988.
9. Dagher FE, Yared GM. Comparison of three files to prepare curved root canal. *J Endod* 21:264-265, 1995.
10. Glosson CR, Haller RH, Dove SB, Rio CE. A comparison of root canal preparation using Ni-Ti hand, Ni-Ti engine-driven, and K-flex endodontic instruments. *J Endod* 21:146-151, 1995.
11. Hur YJ, Kim SK. Change in root canal configuration using different file types and techniques. *J Kor Acad Conserv Dent* 22:291-304, 1997.
12. Schneider SW. A comparison of canal preparations in straight and curved root canals. *Oral Surg Oral Med Oral Pathol* 32:271-275, 1971.
13. Caldwell JL. Change on working length following instrumentation of molar canals. *Oral Surg Oral Med Oral Pathol* 41:114-8, 1976.
14. Faber JP, Bernstein M. The effect of instrumentation on root canal length as measured with an electronic device. *J Endod* 9:114-115, 1983.
15. Kim BH, Kim YS, Lee YK. Working length change by instrumentation according to the canal curvature. *J Kor Acad Conserv Dent* 24:623-627, 1999.
16. Schroeder KP, Walton RE, Rivera EM. Straight line access and coronal flaring: Effect on canal length. *J Endod* 28:474-476, 2002.
17. Davis RD, Marshall JG, Baumgartner JC. Effect of early coronal flaring on working length change in curved canals using rotary nickel-titanium versus stainless steel instruments. *J Endod* 28:438-442, 2002.
18. Thompson SA, Dummer PM. Shaping ability of Profile .04 taper series 29 rotary nickel-titanium instruments in simulated root canals: Part 1. *Int Endod J* 30:1-7, 1997.
19. Thompson SA, Dummer PM. Shaping ability of Hero 642 rotary nickel-titanium instruments in simulated root canals: Part 1. *Int Endod J* 33:248-254, 2000.
20. Bryant ST, Dummer PM, Pitoni C, Bourba M, Moghal S. Shaping ability of .04 and .06 taper Profile rotary nickel-titanium instruments in simulated root canals. *Int Endod J* 32:155-164, 1999.
21. Bryant ST, Thompson SA, Al-Omari MA, Dummer PM. Shaping ability of Profile rotary nickel-titanium instruments with ISO sized tips in simulated root canals: Part 1. *Int Endod J* 31:275-281, 1998.
22. Kum KY, Spangberg L, Cha BY, Jung IY, Lee Sj, Lee CY. Shaping ability of three Profile rotary instrumentation techniques in simulated resin root canals. *J Endod* 26:719-723, 2000.
23. Arens DE, Senia SE, Johnson B, McSpadden J. The crown-down technique: a paradigm shift. interviewed by Donald E. Arens. *Dent Today* 15:38-47, 1996.
24. Yun HH and Kim SK. A comparison of the shaping abilities of four rotary nickel-titanium instruments in simulated root canals. *Oral Surg Oral Med Oral Pathol Endodont Dent Radiol* 95:228-233, 2003.
25. Seok-Dong Choi, Myung-Uk Jin, Ki-Ok Kim, Sung Kyo Kim. Shaping ability of four rotary nickel-titanium instruments to prepare root canal at danger zone. *J Kor Acad Conserv Dent* 29(5):446-453, 2004.

## 국문초록

### 만곡근관에서 근관형성방법에 따른 근관작업장의 변화

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만곡근관에서 근관형성방법에 따른 근관작업장 변화를 평가하기 위하여 발거된 대구치의 협측 또는 근심 근관 40개에서 스테인레스-스틸 수동 파일 (MANI®, 일본), 니켈-티타늄 수동 파일 (Naviflex NT™, 미국), ProFile®, 또는 ProTaper™ (Dentsply-Maillefer, 스위스)를 사용하여 crown-down 방법으로 30번 크기까지 근관을 형성하고 근관형성 전후의 근관작업장 및 만곡도의 변화를 관찰하였다. 근단공에 대한 10-K 파일 끝의 위치변화를 AutoCAD2000 (Autodesk 사, 미국)으로 측정하고 일원변량분석법 및 Tukey's studentized range test로 통계 분석하였다.

모든 군에서 근관형성후 근관장 및 만곡도가 유의하게 감소하였으며, 치관부 근관형성시 Gates Glidden bur를 사용한 수동파일 군이 ProFile 군보다 유의하게 많은 근관장 감소를 초래하였고, 치관부 및 근단부 전체 근관형성후에는 스테인레스 스틸 수동파일 군이 ProFile 군에서보다 유의하게 많은 근관장 감소를 나타내었다 ( $p < 0.05$ ).

**주요어:** 근관작업장, 만곡근관, 수동기구, 전동기구, ProFile, 근관만곡