## The Pulsed I<sub>d</sub>-V<sub>g</sub> methodology and Its Application to the Electron Trapping Characterization of High-κ gate Dielectrics

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Abstract—Pulsed current-voltage (I-V) methods are introduced to evaluate the impact of fast transient charge trapping on the performance of high- $\kappa$  dielectric transistors. Several pulsed I-V measurement configurations and measurement requirements are critically reviewed. Properly configured pulsed I-V measurements are shown to be capable of extracting such device characteristics as trap-free mobility, trapinduced threshold voltage shift ( $\Delta V_t$ ), as well as effective fast transient trap density. The results demonstrate that the pulsed I-V measurements are an essential technique for evaluating high- $\kappa$  gate dielectric devices.

*Index Terms*—High-к, pulse I-V, threshold voltage instability, fast transient charge trapping, mobility, bias temperature instability, hafnium, MOSFET

### **I. INTRODUCTION**

Since silicon dioxide gate dielectric thickness continues to be scaled, gate leakage current may exceed the required specification limits for future technology nodes. To circumvent this issue, higher permittivity ( $\kappa$ ) gate dielectrics, which allow thicker dielectric layers at the same equivalent oxide thickness (EOT), have been introduced [1]. This new class of gate dielectrics requires new measurement methods and analysis. In particular, hafnium (Hf)-based oxides, which are being widely accepted as a leading candidate for high- $\kappa$  gate dielectrics [1], exhibits high density of as-grown structural defects [2-16], some representing electron traps that complicate the evaluation of "intrinsic" performance in high-k gate stacks.

The electron charge trapping process potentially causes threshold voltage instability, mobility degradation, and poor reliability and performance, which are some of the primary issues affecting the use of Hf-based materials in production [17-65]. While significant progress has been made in fabricating high- $\kappa$  gate stacks with less charge trapping [66-69], pulse-based characterization techniques [30, 70-73] remain critically important in understanding charge trapping processes for low power applications, memory cells, etc. This review addresses pulsed current-voltage (I-V) characterization and analysis approaches.

### **II. FAST TRANSIENT CHARGE TRAPPING**

Hf-based high- $\kappa$  gate dielectrics exhibit a phenomenon known as the fast transient charging effect (FTCE) [37]. This effect is caused by substrate electrons injected to and captured by shallow traps (just below the Hf-based dielectric conduction band, Fig. 1) [74], where the trapping may occur within hundreds of nanoseconds to microseconds [50, 73]. The charges trapped during this process are well-localized within the dielectric, with their spatial distribution through the dielectric thickness being determined by the Fermi energy of the channel electrons and the trap energy (presumably, a neutral or singlecharged negative oxygen vacancies) [4, 7, 9-11, 16]. The

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**Fig. 1.** Band diagram schematic for the electron trapping process during pulsed I-V measurements. Inset: Two scenarios are shown: when the pulse time  $t_p$  (sum of  $t_r$  and pulse width) is much shorter and longer than the trapping time  $\tau_c$ . The latter defines the onset of electron trapping into the high- $\kappa$  bulk.

fast trapping, which is reversible with no residual damage [30, 75, 76], can contribute significantly to threshold voltage  $(V_t)$  instability and degradation of device performance in Hf-based gate stack nMOS transistors.

pMOS Hf-based transistors, on the other hand, typically exhibit negligible fast transient charging (FTC) [33, 77] in inversion due to a lack of defect states with the appropriate energies. An example is shown in Fig. 2 for an inversion bias of  $V_g = -2$  V with a standard midgap work function metal electrode illustrating that the FTC sites are far away from any resonant injection with the gate or substrate injection points. If significant FTC is detected, the test set-up or measurement may have issues [73] (should not be confused with NBTI measurements, which may have a fast component).

Because conventional DC characterization can be



**Fig. 2.** Band diagram schematic for a pMOS gate stack illustrating injected electrons from the gate are not in resonance with the FTC trap sites, thereby demonstrating that negligible FTC occurs in pMOS devices.

adversely affected by FTC while the DC measurement is being conducted, thus lowering the drive current (Fig. 3(a)), the pulsed I-V methodology was introduced to quantify the transient charge trapping as well as to measure "intrinsic" (i.e., trapping-free) device characteristics [30, 70-72].



**Fig. 3.** Various forms of pulsed  $I_d$  data in the (a) pulse voltage, or (b) time domains based on the "ramped" pulse or "single" pulse (dashed box) illustration in (c). Results clearly show that  $I_d$  degrades at the top of the pulse (i.e., pulse width portion) due to FTC while the ramped pulse  $I_d$  and the  $t_r$  portion coincide to demonstrate trapping-free characteristics. DC  $I_d$ -V<sub>g</sub> is included for comparison.

## III. MEASUREMENT TECHNIQUE AND INSTRUMENTATION CONFIGURATIONS

#### 1. Measurement Technique

Pulsed drain current-gate voltage  $(I_d-V_g)$  measurements are usually performed by applying a trapezoidal (e.g., rise time, pulse width, and fall time) or triangular (e.g., rise and fall time only)  $V_g$  pulse on the gate of a transistor configured as an inverter and then measuring  $I_d$ . While a voltage pulse is applied to the gate of the FET, the  $V_g$  and drain voltage (V<sub>d</sub>) are simultaneously recorded on a digital storage oscilloscope. The drain voltage response is converted to  $I_d$  and plotted against the pulse bias,  $V_g$ , or pulse time. From the  $V_d$  response,  $I_d$  (in the linear regime) can be calculated as [78]

$$I_d = \frac{V_{dd}}{V_d} \left( \frac{V_{dd} - V_d}{R_L} \right) \tag{1}$$

where  $V_{dd}$  is the drain voltage,  $V_d$  is the drain response voltage, and  $R_L$  is the load resistance.

Figs. 3(a) and 3(b) illustrate  $I_d$ - $V_g$  (pulse voltage domain) and  $I_d$ -time (pulse time domain) characteristics, respectively, wherein the change of  $I_d$  during a "single" pulse measurement can be determined. The dashed box in Fig. 3(c) illustrates the "single" pulse wherein the  $V_g$  pulse with its corresponding  $V_d$  response is captured and converted into  $I_d$ - $V_g$  or  $I_d$ -time. From this, the hysteresis in the  $I_d$ - $V_g$  curve (Fig. 3(a)) or the decrease of  $I_d$  in the  $I_d$ -time plot (Fig. 3(b)) illustrates the threshold voltage change due to charge trapping.

Another approach to the pulsed I-V technique is the "ramped pulse" I-V (Fig. 3(a)), which generates a complete  $I_d$ -V<sub>g</sub> curve within the total "single" pulse V<sub>g</sub> range by applying multiple pulses with incrementally rising amplitude  $V_g$  up to  $V_g = V_{g,max}$  and extracting  $I_d$  at each V<sub>g</sub> value (Fig. 3(c)) [33, 72]. The advantage of this approach is that each pulse can have a very short characteristic time (around 37 ns = rise time + pulse width with ~0.1% duty cycle in this work), allowing "intrinsic" Id values to be obtained. It also provides better resolution by averaging the response pulse V<sub>d</sub> values during a portion of the pulse width time, thereby reducing the effect of fluctuations. Comparing this approach to the "single" pulse method (see Fig. 3(a)) revealed that a 5 µs rise time in the single pulse measurement is short enough to obtain the trapping-free I<sub>d</sub> characteristic in this particular gate stack due to the 1 nm SiO<sub>2</sub> interfacial layer since both techniques coincide on the "trapping-free" portion of the I<sub>d</sub>-V<sub>g</sub>.

In summary, the "ramped pulse" approach executes a truly trap-free  $I_d$ - $V_g$  curve, which is vital, for instance, for extracting intrinsic mobility [79]. However, because it is ultra-fast, this methodology does not allow the amount of trapping that can occur in the gate stack to be quantified. Therefore, the "single" pulse measurement should be used to study charge trapping. To obtain a

correct charge trapping quantity, the rise time portion in the "single" pulse measurement must coincide with the ultra-short, "ramped" pulse one. In the (I<sub>d</sub>-time) domain, the "single" pulse approach also delivers information on the charge trapping kinetics. This is the method used to obtain  $\Delta V_t$ , explained in section V-1.

### 2. Instrumentation Configurations

Four basic test set-up configurations have been employed to execute many of the pulse-based methodologies reported in the literature [30, 70-72]. In two of these configurations, the MOSFET is operated in an inverter circuit with a load resistor arranged in two ways: 1) a standard resistor placed in series between V<sub>dd</sub> and the drain of the MOSFET as shown in Fig. 4(a) [30], or 2) the 50  $\Omega$  environment of a radio frequency (RF) set-up (Fig. 4(b)) [72]. The third configuration, shown in Fig. 4(c), incorporates an operational amplifier (op-amp) [71] that takes advantage of the virtual short circuit property of op-amp operation. This allows the drain current to be measured across the sense resistor, R. The fourth measurement incorporates a current amplifier in series between common ground and the source of the MOSFET (Fig. 4(d)) [70].

### A. "Conventional" set-up

This configuration is a straightforward approach to setting up a pulsed  $I_d$ - $V_g$  measurement because it can be built using "standard" lab equipment and cables (Fig. 4(a)) [30]. This configuration can facilitate measurements typically within tens of microseconds when conducting the  $I_d$ - $V_g$  form of the measurement [30]. The time limitation is caused by not having a true radio frequency (RF)-capable configuration. Explicit and quantifiable limitations can be found in [71]. However, simply using a small dimension device (e.g., W/L = 10/1 µm or smaller) and relatively short cables will enable measurements in the tens of microseconds regime.

### B. Ultra-Short Pulsed I-V set-up

This configuration requires RF-capable instrumentation and test structures to achieve optimum measurement performance with nanosecond regime timing. The



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**Fig. 4.** (a) Schematic illustration of the measurement setup used for pulsed  $I_d - V_g$  experiments in the µs range; (b) Experimental set-up for the ultra-short pulsed I-V measurement illustrating signal propagation paths (1 and 2) that should be equal in length and the internal circuitry of a conventional bias tee consisting of an inductor and capacitor; (c) custom op-amp circuit that takes advantage of the "virtual short" property of the op-amp to mitigate the charging and discharging of parasitic capacitance; (d) current amplifier configuration with the current amplifier placed between source and ground with  $V_{dd}$  applied to the drain.

approach still operates with the device under test in an inverter circuit, but uses the 50  $\Omega$  environment as the load resistor. The difference in the experimental set-up is shown in Fig. 4(b) [72]. K. Jenkins, et al., first introduced this type of measurement configuration [80]. Bias tees present a critical component in this RF set-up due to the 50  $\Omega$  environment. The schematically shown bias tee in Fig. 4(b) isolates the AC and DC signals intended for the oscilloscope and transistor drain, respectively, from each other. Note that the characteristic charging time of the internal capacitor in the bias tee may limit the upper range of the pulse width while the minimum current resolution is limited by the voltage resolution of the scope at the smallest range divided by 50  $\Omega$ . The set-up discussed here also permits a pulsed I<sub>d</sub>-V<sub>d</sub> capability due to the two bias tees used in the measurement set-up (Fig. 4(b)) without having to change the test set-up configuration [33, 73]. The "pick-off" tee used in the gate circuit in Fig. 4(b) allows the gate pulse voltage to be monitored non-intrusively. More configuration details can be found in [73]. A potential limiter of this technique is the need for RF timescale equipment and test structures. In addition, this ultra-fast measurement typically measures a completely trap-free result, which does not allow levels of fast transient trapping to be quantified. However, it should serve as a benchmark for all other pulse measurements to ensure an accurate FTCE analysis (see section V. 1.).

### C. Operational Amplifier/Current Amplifier Set-up

This configuration has been achieved in two ways: a) a custom design using a standard op-amp circuit (Fig. 4(c)) [71], and 4(b) a current amplifier (Fig. 4(d)) [70].

The custom-designed op-amp circuitry takes advantage of the short circuit property of the op-amp in which the voltage of the two inputs is expected to be equal. The fixed  $V_{dd}$  applied to the drain is provided by the voltage source; therefore, the parasitic capacitance,  $C_o$ , does not charging or discharge [71]. The measured output voltage captured from the oscilloscope is linked to I<sub>d</sub> through the following expression [71]:

$$V_{out} = \left(I_d - I_{gd}\right) \cdot R + V_{ds} \tag{2}$$

where Igd is the gate-to-drain current through the parasitic

capacitor ( $C_{gd}$ ),  $V_{ds}$  is the drain voltage, and R is the sense resistance. Because the  $C_{gd}$  is weak in short channel devices,  $I_{gd}$  is negligible compared to the drain current, thereby allowing  $I_d$  to be extracted. The limiting factor for the time resolution of this configuration is determined by the bandwidth of the op-amp. Further set-up details can be found in [71].

The current amplifier, placed in series between ground and the source terminal while  $V_{dd}$  is applied to the drain, provides a relatively simple way to make the pulsed  $I_{d}$ - $V_{g}$  measurement when a  $V_{g}$  pulse is applied to the gate of the MOSFET [70]. Similar to the op-amp circuit, the time resolution for this configuration is determined by the bandwidth of the op-amp.

### **IV. MEASUREMENT REQUIREMENTS**

Several key components must be implemented to ensure robust measurement execution, otherwise significant errors can occur that will impact the extracted signals that are captured and stored on the digital oscilloscope. First, the trapezoidal or triangular pulse should start and end at a discharge condition. For the FTCE, reversibility of this effect was found to be at a discharge voltage of -1V [30, 75, 76]. In addition, a very low duty cycle (e.g.,  $\leq 0.1$  %) should be implemented. This allows the device under test to essentially be in an "off"/discharge condition most of the time and "on" for extremely short times. This way the "single" pulse can actually be a standard pulse train, allowing averaging if better resolution is desired and/or required to avoid fluctuations.

When using the measurement in the  $I_d$ - $V_g$  form (Fig. 3(a)), the input pulse (i.e.,  $V_g$  pulse) must be synchronized with the output response (i.e., response at the  $V_d$  node, dashed box, of Fig. 3(c)). To achieve this, the signal "paths" must take the same propagation time to traverse the path and simultaneously arrive at the oscilloscope. This is achieved by having the same cable length path for the  $V_g$  input and  $V_d$  response and by having an oscilloscope that can effectively remove any remaining propagation delay (e.g., paths 1 and 2 in Fig. 4(b)) [73, 81]. If this is not done, a measurement error could occur at the minimum frequency/time range of the particular pulse set-up. The error can manifest itself as a false hysteresis as shown in Fig. 5. This 2 nm HfO<sub>2</sub> gate stack,



**Fig. 5.** Single pulsed I-V data illustrating a hysteresis artifact  $(\Delta V_t)$  in the I<sub>d</sub>-V<sub>g</sub> domain (a) while no detectable charging (i.e., I<sub>d</sub> degradation) is observed in the time domain, (b). The measurement set-up limitation is verified by the artificial hysteresis on conventional SiO<sub>2</sub>, which does not exhibit the FTCE (insets).

which has not suffered from significant FTC [66, 69, 82], should not exhibit any hysteresis. However, Fig. 5a clearly illustrates a small hysteresis, although the I<sub>d</sub>-time data (Fig. 5(b)) shows no decay in the pulse width portion. The inset results exhibit a V<sub>t</sub> shift artifact for a fast trapping-free SiO<sub>2</sub> sample (insets, Fig. 5) as well, confirming the hysteresis is not real. Therefore, estimating  $\Delta V_t$  as a shift between I<sub>d</sub>-V<sub>g</sub> traces corresponding to the rise and fall of the pulse bias may not be accurate [70, 83, 84] when a non-optimized measurement set-up is used.

### V. APPLICATIONS

The pulsed I-V methodology can be used for more than just measuring the "intrinsic" drive current performance in the absence of FTC. Proper analysis techniques can provide information on charge trapping [32, 70-74, 81, 83, 85] and the effect on device performance, separation of fast and slow trapping processes [20, 32, 50, 54, 55, 74, 86], and bias temperature instability [50, 87-90].

# 1. Quantifying Trapped Charge and Its Effects on Device Performance

Using pulsed  $I_d$ -time [30, 33, 73, 83] or a correction technique for pulsed  $I_d$ -V<sub>g</sub> can circumvent the issues discussed in section IV [81]. In the case of  $I_d$ -time, very

fast rise and fall times can be used since propagation delay is not an issue. The V<sub>d</sub> response is plotted against time instead of the input V<sub>g</sub> pulse. The degradation in I<sub>d</sub> with time is reflected in the fast transient charge trapping. The threshold voltage shift,  $\Delta V_t$ , can be determined from the change in I<sub>d</sub> through the expression [83, 91]

$$\Delta V_t = \frac{\Delta I_d}{I_d} \left( V_g - V_t \right) \tag{3}$$

where  $\Delta I_d$  is the  $I_d$  degradation between the start and end of the V<sub>g</sub> pulse width,  $I_d$  is the maximum  $I_d$  before transient charging,  $V_g$  is the pulse amplitude applied to the gate, and  $V_t$  is the threshold voltage. The approximation used in Eq. (3) is applicable when mobility does not decrease significantly due to a high vertical field in the channel caused by high gate bias (i.e., when V<sub>g</sub> is so high that the slope of the I<sub>d</sub>(V<sub>g</sub>) curve decreases significantly from its maximum value corresponding to maximum transconductance, g<sub>m.max</sub>) [81].

Fig. 6 illustrates pulsed mobility extracted (to be discussed in section V-1, part A) from the rise (i.e., trapping-free) and fall (i.e., after trapping) time portions showing similar effective mobility values. Even after 100  $\mu$ s of charging time, the falling I<sub>d</sub>-V<sub>g</sub> curve appears to be parallel to the rising curve suggesting no significant impact due to remote coulomb scattering from the trapped electrons (Fig. 6, inset), which confirms the



**Fig. 6.** Similar mobility values extracted from the rise (trapfree) and fall (after trapping) portions of the single pulse measurement (inset, a) demonstrating that remote coulomb scattering is negligible in high- $\kappa$  gate stacks due to bulk trapping beyond the 1 nm SiO<sub>2</sub>-like interfacial layer.

applicability of Eq. (3) to this particular gate stack. The negligible effect of the trapped electrons on intrinsic mobility can be understood when one considers that the trapped charges are located in the bulk of the high- $\kappa$  [76, 79], relatively far from the channel.

Therefore, similar pulse data in Fig. 3 can be used as an example of measurements where Eq. (3) is applicable:  $\Delta V_t$  obtained from the data in Fig. 3(b) using Eq. (3) is equal to the hysteresis value extracted from Fig. 3(a). A precise expression for  $\Delta V_t$ , which takes into account variation of the mobility value with changing threshold voltage, is given in [83]. With this extraction procedure for  $\Delta V_t$ , the onset of FTCE can be evaluated [33]. Fig. 7 demonstrates the two extremes, with ( $t_p > \tau_c$ ) and without ( $t_p << \tau_c$ ) FTC, for a sample with significant trapping, as illustrated in Fig. 1. By applying pulses with a  $t_p$ magnitude between these extreme values, the onset of trapping,  $\tau_c$ , can be determined.

For any pulsed I-V measurement, the pulse rise time plus its width represents the charging time,  $t_p$ . To ensure the absence of FTCE, the pulse charging time must be shorter than the onset of the trapping time,  $\tau_c$ . This is schematically illustrated in Fig. 1 (inset), which includes two extreme cases of I<sub>d,sat</sub> current measured with ultrashort ( $t_p \ll \tau_c$ ) and long pulse times. Fig. 8 shows an example of the effect of the pulse rising time (charging time) on I<sub>d</sub> [73]. Dependence on the pulse rising times reflects on the charging at higher V<sub>g</sub> values. Significant charging during the pulse rising time may result in FTCE being underestimated. Therefore, a measurement capability



**Fig. 7.** Pulse  $I_d$  dependence on the charging time  $t_p$  when (a)  $t_p \approx \tau_c$  (no electron trapping), and (b)  $t_p \gg \tau_c$  (electron trapping is proportional to  $\Delta I_d$ ).



Fig. 8. Single pulsed I-V measurements on high- $\kappa$  demonstrating the impact of the pulse rise time on charging. A fast enough rise time (i.e., short t<sub>r</sub>) ensures a "trap-free" drain current.

that ensures a trapping-free characteristic throughout the entire pulse measurement is required to guarantee no FTCE. In addition, highly scaled interfacial layers in high- $\kappa$  gate stacks may exhibit very fast trapping, which would require pulse measurements below the microsecond regime (Fig. 8). This can be achieved by using the ultrashort pulsed I-V set-up in Fig. 4(b). Furthermore, this is a potentially powerful measurement technique for characterizing high- $\kappa$  gate stacks on silicon-on-insulators when self-heating effects should also be eliminated to achieve intrinsic device performance [80].

Another approach, which uses the pulsed  $I_d$ - $V_g$  hysteresis, can be employed when the limitations of being able to use eq. (3) have been exceeded (Fig. 9) [81]. This approach effectively negates the propagation delay by intentionally introducing a phase delay time between



Fig. 9. The effect of phase delay time between the two input channels of the oscilloscope on the measured hysteresis of the  $I_d$ - $V_g$  curves in a single pulse measurement.

the two channels of the oscilloscope. To obtain the accurate phase delay time to compensate for the propagation delay, Id-Vg curves generated by "short" and "long" triangle pulses with equal rise and fall times, should be compared (Fig. 9). Three different phase delay times ranging from zero to 20 ns were used in both short (thick curves) and long (thin curves) pulses. It can be seen that the I<sub>d</sub>-V<sub>g</sub> curves generated by the short pulses are strongly affected by the phase delay times, which result in different I<sub>d</sub>-V<sub>g</sub> hysteresis values. On the other hand, the complete overlap of the long pulse curves obtained with different delay times indicates that the phase delay times in the ns range have no effect on the pulse in the us range. Therefore, by varying the phase delay time in the short pulse measurement to match the  $I_d$ - $V_g$  curves of the short and long pulses within the voltage range for  $V_g$  less than  $V_t$  (where no FTCE takes place), the correct phase delay time that compensates the signal delay due to different propagation paths for the given pulse measurement set-up can be determined.

### A. Impact of Dielectric Properties on Fast Transient Charge Trapping

Typical high- $\kappa$  gate stack structures are comprised of two layers: an interfacial layer and a high- $\kappa$  layer (Fig. 1). During gate stack fabrication, the interfacial layer can be engineered or it can grow spontaneously [33, 78, 92, 93]. The FTCE can be influenced by these two layers as well as by the amount of hafnium in the high- $\kappa$  layer.

Effects of the interfacial layer thickness, physical thickness of the high-k dielectric, and its Hf content on the fast electron trapping process were evaluated by using a combination of the ultra-fast pulse technique described above (covering the range up to 100 ns) and the conventional "single" pulse (covering the range between 100 ns to 6 ms) [30, 76, 94]. The effect of interfacial layer thickness is demonstrated in Figs. 10-12. Since the trap sites in the high- $\kappa$  layer are filled by tunneling from the inversion layer through the interfacial layer (Fig. 1), a thinner interface leads to a stronger tunneling current and, hence, greater electron trapping. Accordingly, critical time (the pulse width at which the onset of trapping occurs),  $\tau_c$ , decreases and the V<sub>t</sub> shift increases for thinner interfacial oxides (Fig. 10). The impact of electron trapping on DC mobility is shown in



**Fig. 10.** Normalized  $\Delta V_t$  for varying IL thicknesses. Thicker IL increases the tunneling distance (see Fig. 1) to available traps, thereby increasing  $\tau_c$ .



**Fig. 11.** Correlation of  $V_t$  shift (trapped charge) to the extracted DC mobility illustrating degraded mobility as the IL becomes thinner.



**Fig. 12.** Expected mobility increase (thinner IL  $\rightarrow$  larger pulse/DC I<sub>d,lin</sub> ratio) as a function of interfacial layer thickness compared with the onset of the critical time,  $\tau_c$ .

Fig. 11 where the DC mobility increases as the  $\Delta V_t$  values, calculated based on the  $\Delta I_d$  [83, 91], diminish in proportion to the thickness of interfacial layer.

A mobility increase (which may be expected if the fast

charge trapping is eliminated), called "expected mobility," was estimated from the ratio of  $I_{d,lin}$  values measured in the pulse and DC regimes (Figs. 11 and 12).

For samples of different  $HfSi_xO_y$  (20% SiO<sub>2</sub>) physical thicknesses of 3, 5, and 7 nm, all with a TiN electrode, the interfacial layer was fixed at ~1 nm SiO<sub>2</sub>. As the physical thickness of the dielectric increases, the total number of traps accessible at the given applied bias also increases, or the filled trap location shifts towards the device channel, resulting in a greater V<sub>t</sub> shift [76] (Fig. 13) that correlates with the degradation of the electron mobility (Fig. 14).

Hafnium content has an apparent influence on both the electron trapping and  $\tau_c$  (Figs. 15 and 16). The  $\Delta V_t$  increases with the Hf content indicating that electron traps may be associated with the Hf atoms.



Fig. 13.  $\Delta V_t$  for various high- $\kappa$  physical thicknesses. Physically thicker high- $\kappa$  is subject to faster and more severe charge trapping.



**Fig. 14.** Expected mobility increase (thinner high- $k \rightarrow$  larger pulse/DC I<sub>d,lin</sub> ratio) as a function of high- $\kappa$  layer thickness compared with the onset of the critical time,  $\tau_c$ .



Fig. 15. Normalized  $\Delta V_t$  for various hafnium contents. More Hf results in faster and greater charge trapping.



Fig. 16. An increase in DC  $\Delta V_t$  and the corresponding decrease in DC mobility as the Hf content increases.

### B. Factors Controlling V<sub>t</sub> shift

In the pulsed I-V measurement, the effect of the trapped charge on  $\Delta V_t$  is primarily determined by the  $V_g$  pulse conditions. The  $V_g$  pulse amplitude affects both the magnitude of the injection current and the point of injection (the charge trapping location) in the dielectric. To understand the major factors controlling  $\Delta V_t$ —charge supply or trapping location with respect to the gate electrode—the pulse width was fixed at 100 µs and the pulse  $V_g$  (i.e., pulse height) was varied to study the bias dependence [73].

It has been demonstrated that the fast trapping process, with a characteristic time of about 100  $\mu$ s, is independent of temperature, implying that the pre-existing traps are filled by the resonant capture of the tunneling electron injected from the substrate [20, 74]. The charges trapped by this process are well-localized within the dielectric thickness, with their location being determined by the

Fermi energy of the channel electrons and the trap energy, whose value is close to the  $HfO_2$  conduction band edge, Fig. 1 (presumably, a neutral or single-charged negative oxygen vacancy) [4, 7, 9-11, 16]. Therefore, we assume for simplicity that the traps are characterized by a single energy value that is close to the bottom of the conduction band [4, 20, 74]. For longer stress times, over 1 second, the trapped charge distribution widens due to slow temperature-activated electron capture processes [50, 74].

The obtained dependences of  $\Delta V_t$  vs. injected charge, Fig. 17, show no correlation, indicating that fast transient charging is not a charge supply-driven phenomenon. evaluate the impact of the position of the trapped charge on  $\Delta V_t$ , band diagrams were constructed, as shown in the examples in Fig. 18, based on the physical thicknesses and  $\kappa$  values of each layer in the different bi-layer stacks under investigation. The band diagrams were generated for various Vg pulses using the software developed by Boise State University [95]. Then, at the given V<sub>g</sub>, the location of the trapped charge is defined by the resonance between the Fermi level in the substrate and the energy level of the pre-existing traps in the Hf-based dielectric [50, 74]. Knowing the distance of the trapped charge from the gate electrode allows the trap charge density to be calculated by

$$N_{trap} = \frac{\varepsilon_o \cdot \kappa \cdot \Delta V_t}{q \cdot x} \tag{4}$$



Fig. 17.  $\Delta V_t$  vs. the injected charge,  $Q_{inj}$  illustrating no correlation between the  $\Delta V_t$  and injected charge.



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**Fig. 18.** The gate stack energy band diagrams for (a) 1.1 nm  $SiO_2/5$  nm HfSiO and (b) 1.1 nm  $SiO_2/3$  nm HfO<sub>2</sub> for various pulsed V<sub>g</sub> values. An example of the resonant electron trapping location with respect to the Fermi level for V<sub>g</sub> = 1.6 V is shown.

where  $\Delta V_t$  is the extracted threshold voltage shift, *x* is the experimentally extracted distance from the gate electrode (example, Fig. 18(a)), *q* is the fundamental electron charge,  $\varepsilon_o$  is the permittivity of free space, and  $\kappa$  is the dielectric constant of the high- $\kappa$  layer. (For more details on the assumptions and limitations of this trap density extraction procedure, see [73].)

By changing  $V_g$ , one can obtain x and thus the trap density profile across the thickness of the high- $\kappa$  film using Eq. (4). While the position x at each given pulse voltage may not be defined exactly, the measurements still allow the relative distribution of x values to be extracted in a self-consistent way. Fig. 19 shows the



Fig. 19. Defect density profile of different high- $\kappa$  gate stacks calculated using the resonant trap location distance referenced from the gate electrode (Fig. 18) for the corresponding V<sub>g</sub> pulse value.

defect profiles for several gate stacks. Within the referenced assumptions, uniform trap density profiles were obtained in all gate stacks analyzed in this study. As follows, the observed increase of  $\Delta V_t$  with the pulse amplitude is due to the trapped charge being closer to the substrate rather than the amount of the trapped charge being greater.

In summary, this approach probes each sample through its high- $\kappa$  thickness by changing the measurement pulse voltage, thereby changing the band bending (i.e., resonant trapping point), which allows trap density information to be directly extracted at each point in the given sample [73].

### C. The Effect of FTC on Channel Mobility

In the linear regime, the FTCE can significantly impact mobility [31, 63, 64, 66, 79, 83, 91, 92, 96-98]. In a conventional DC sweep of the Id-Vg measurement, the threshold voltage shifts as the measurement progresses, thereby decreasing the drive current at each bias sweep point resulting in decreased mobility. Several FTC correction techniques discussed in the literature can correct for this effect [31, 63, 79, 83]. One technique that requires only two measurements and minimal data analysis was presented in [79]. In this approach, pulsed I<sub>d</sub>-V<sub>g</sub> is combined with North Carolina State University's CVC [99] and mob2d [100] modeling parameter extraction software. To extract mobility, mob2d performs a non-linear, least squares fit to experimental pulsed I<sub>d</sub> data in conjunction with the EOT and substrate doping supplied from CVC. EOT and substrate doping are negligibly impacted by FTC [101]. Therefore, the result is a trap-free mobility extraction. Fig. 20 illustrates the impact of trapped charge in the DC mobility data compared to the trap-free, pulsed-based extraction for the  $I_d$ - $V_g$  data in the inset where the pulse-based mobility is higher than its DC-based counterpart [32, 80]. Fig. 21 compares the pulse and DC mobility extractions using CVC and mob2d for high-k gate stacks with different interfacial layer (IL) thicknesses. The sample with a 1.9 nm SiO<sub>2</sub> interfacial layer exhibits essentially the same DC and pulsed mobility since fast transient charging is negligible in thick interfaces (quite similar DC and pulsed I<sub>d</sub>-V<sub>g</sub> curves – not shown). As the interface becomes thinner, the difference between the pulsed and

![](_page_10_Figure_1.jpeg)

Fig. 20. Comparison of DC mobility to the novel pulse mobility technique for the  $I_d$ -V<sub>g</sub> data in the inset. The mobility values extracted using the proposed mob2d pulse methodology and the direct measurement of N<sub>inv</sub> technique [32] show excellent agreement.

![](_page_10_Figure_3.jpeg)

**Fig. 21.** Application of the pulse mobility extraction method [80] to gate stacks with interfacial layers (IL) of varying thicknesses and fixed  $HfSiO_x$  dielectric layer.

DC mobility for a given gate stack becomes greater. The overall degradation in the pulsed (intrinsic) mobility as the interface layer becomes thinner can be attributed to poorer interfacial layer quality [102] and greater effects of soft optical phonons [64] and crystallinity [21, 103].

### D. Fast Transient Trapped Charge Relaxation

Reports have shown that, in addition to FTC, high- $\kappa$  gate dielectrics also demonstrate fast relaxation of the trapped charge, although on a slightly longer time scale [88, 104]. Fig. 22 illustrates this fast relaxation phenolmenon. After a two-level V<sub>g</sub> pulse (Fig. 22 inset: the high level is in strong inversion, and the low level is just above  $V_t$ ) the drain current recovers due to relaxation (charge detrapping) at this low  $V_g$  level in ~ 150 µs. Fig. 23 demonstrates that the trapped charge can return to the DC measurement results in as little as 250 µs.

![](_page_10_Figure_9.jpeg)

Fig. 22. Illustration of fast transient charge trapping ( $I_d$  decay) and detrapping ( $I_d$  recovery) for the  $V_g$  pulse in the inset.

![](_page_10_Figure_11.jpeg)

Fig. 23.  $V_t$  shifts immediately after the 100  $\mu$ s stress and after 250  $\mu$ s of post-stress relaxation compared to conventional "stress and sense" approach.

## 2. Implications of Fast Transient Trapping and Detrapping During Stress Measurements

Note that since fast trapping and recovery can occur in high- $\kappa$  gate stack transistors, it significantly impacts positive bias temperature instability with an adverse effect on the lifetime projection [87, 88]. Fast recovery can occur between the stress and "sense" (i.e., monitoring parameter measurement) of conventional constant voltage stress with interspersed DC I<sub>d</sub>-V<sub>g</sub> measurements (V<sub>t</sub> extraction) due to the interval between the removal of the stress and the subsequent "sense" I<sub>d</sub>-V<sub>g</sub>

measurement. This can lead to significant underestimation of the  $V_t$  shift [22, 25, 32, 84, 89, 90, 105, 106]. Therefore, the time delay between the stress and measurement must be shortened.

### A. Effect of Relaxation and Its Impact on the Lifetime Projection

Several techniques have been introduced in the literature to mitigate the effects of fast relaxation [88, 90, 107]. One of particular interest employs the pulsed I-V methodology [88, 90]. Fig. 24 illustrates the measurement schematic for the pulsed approach vs. conventional DC stress and sense. As Fig. 24(b) shows, the pulsed I-V is measured immediately in the downward pulse from the stress condition, thereby removing any relaxation [88]. To study the impact of fast relaxation on the extraction of  $V_{t}$ , the  $I_{d}$  of the rising trace on the inverted triangular pulse can be extracted after modulating the fall time of the downward portion, which can effectively quantify the relaxation time [88]. The results are shown in Fig. 25 where the quantity of the trapped charge, reflected in the  $V_t$  shift, is similar to the results of the conventional DC approach as the relaxation time increases [88]. Moreover, the slopes (i.e., power law exponents) change significantly with changes in the relaxation time. Therefore, it is worthwhile to separate the effects of the fast relaxation on the time evolution of degradation with stress.

![](_page_11_Figure_5.jpeg)

Fig. 24. The schematic comparison of stress-sense schemes using the stress-interrupted DC  $I_d$ - $V_g$  method and single pulse method.

![](_page_11_Figure_7.jpeg)

Fig. 25.  $\Delta V_t$  dependence on stress time when extracting  $V_t$  from the rising portion of  $V_g$  (see Fig. 24(b)) for different pulse times.

#### B. Separation of Fast and Slow Trapping

In addition to fast transient mechanisms, slow trapping and/or trap generation can impact V<sub>t</sub> instability in high- $\kappa$ transistors when constant voltage stress is measured [22, 25, 30, 34, 84, 88, 89, 105]. The oxygen vacancy defects responsible for the FTCE have also been found to exhibit a temperature-activated slow migration of trapped electrons to unoccupied traps [50, 74]. Fig. 26 illustrates these two components over a long time scale [50]. A temperature-independent feature is detected in fast measurement times (pulsed I-V regime), indicating a direct tunneling mechanism to the neutral or singlecharged negative oxygen vacancy fast transient traps. Then, at longer stress times, a temperature effect is seen when a larger  $\Delta V_t$  is extracted at the higher temperature. The fast relaxation detraps in a similar manner [50].

To remove the effect of the FTC so that only the slow migration and/or trap generation can be studied, the previously mentioned pulsed I-V combined with constant voltage stress and subsequent data analysis was used [88]. A physical model-based subtraction of the initial V<sub>t</sub> (contains only the fast relaxation portion) from each subsequent V<sub>t</sub> point in the time dependence effectively removes the fast transient detrapping component [88]. Fig. 27 shows parallel curves after the initial data point subtraction provides a "universal" slope, which suggests that the dependence of the power law exponent on pulse time is due to fast transient charge detrapping [87]. In addition, Fig. 28 further confirms this universality because different measurement techniques have a very similar

![](_page_12_Figure_1.jpeg)

**Fig. 26.** Fast (temperature-independent) and slow (temperaturedependent) charge trapping processes in typical  $HfO_2$  gate stacks where the fast process pseudo-saturates within 100  $\mu$ s and transitions to the slow process around 10° sec of stressing.

![](_page_12_Figure_3.jpeg)

Fig. 27. The power law dependence after removal of the FTC portion of the V<sub>t</sub> shift (i.e., subtraction of the first  $\Delta V_t$  point from all subsequent points) demonstrating that all curves fall on an intrinsic curve regardless of the sense measurement time.

![](_page_12_Figure_5.jpeg)

Fig. 28. The correlation of  $\Delta V_t$  measured using different characterization methods.

slope (power law exponent) after removing the fast transient effects when measured on the same high-k gate dielectric stack [87].

### **VI.** CONCLUSIONS

Several pulsed I-V measurement configurations have been critically evaluated. The ultra-short pulsed I-V method is found to be the benchmark for determining truly trap-free characteristics of high-κ gate dielectric devices. The pulsed I-V methodology is shown to be capable of obtaining "intrinsic" (i.e., trap-free) performance of hafnium-based gate dielectrics. To evaluate reliability, the pulsed-based approach is required to extract device lifetime, which can be impacted by the fast transient phenomena. However, to ascertain the trap-free results requires a rigorous evaluation of the measurement configuration along with its corresponding analysis. Failing to calibrate the measurement set-up properly (or employing a set-up that is too slow) results in an underestimation of the Vt shift, effective mobility, and trap density.

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![](_page_19_Picture_1.jpeg)

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![](_page_19_Picture_4.jpeg)

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![](_page_19_Picture_7.jpeg)

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![](_page_19_Picture_10.jpeg)

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![](_page_20_Picture_1.jpeg)

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