

Linearization of T-S Fuzzy Systems and Robust Optimal Control

Min Chan Kim, Fa Guang Wang, Seung Kyu Park, Gun Pyong Kwak , Tae Sung Yoon and Ho Kyun Ahn, *Member, KIMICS*

Abstract— This paper proposes a novel linearization method for Takagi-sugeno (TS) fuzzy model. A T-S fuzzy controller consists of linear controllers based on local linear models and the local linear controllers cannot be designed independently because of overall stability conditions which are usually conservative. To use linear control theories easily for T-S fuzzy system, the linearization of T-S fuzzy model is required. However, The linearization of T-S fuzzy model is difficult to be achieved by using existing linearization methods because fuzzy rules and membership functions are included in T-S fuzzy models. So, a new linearization method is proposed for the T-S fuzzy system based on the idea of T-S fuzzy state transformation. For the T-S fuzzy system linearized with uncertainties, a robust optimal controller with the robustness of sliding mode control(SMC) is designed.

Index Terms— T-S fuzzy control, linearization, robust optimal, sliding mode control.

I. INTRODUCTION

T-S fuzzy model is based on using a set of fuzzy rules to describe a global nonlinear system in terms of a set of local linear models which are smoothly connected by fuzzy membership functions. A T-S fuzzy controller is also described by using a set of local linear controllers. A global controller is constructed from the local controllers in such a way that global stability with various performance indexes of the closed-loop fuzzy control system is guaranteed. The major techniques that have been used include quadratic stabilization, linear matrix inequalities (LMIs), Lyapunov stability theory, bilinear matrix inequalities, and so on [1]-[4]. Definitely, T-S fuzzy models provide a basis for development of systematic approaches to stability analysis and controller design of fuzzy control systems in view of powerful conventional control theory and techniques.

However, the requirement of stability condition is conservative for the designing of a T-S fuzzy controller. So, a great deal of attention is focused on the stability

Manuscript received November 2, 2010; revised November 22, 2010; accepted November 30, 2010.

Min-Chan Kim is with the Department of Electrical Engineering, Changwon National University, Changwon, 641-773, Korea (Email: mchkim @changwon.ac.kr)

Seung-Kyu Park is with the Department of Electrical Engineering, Changwon National University, Changwon, 641-773, Korea (Email: skpark @changwon.ac.kr)

analysis of T-S fuzzy system. The requirement of stability conditions and their conservatism makes it difficult to use the linear conventional control techniques for the T-S fuzzy model. This difficulty is more severe in the case of existence of uncertainties and time delay in the T-S fuzzy system [6]-[8]. These difficulties are not shown in control of linear systems. Once the T-S fuzzy models have been linearized, then the conventional linear controllers can be used without such difficulties.

Therefore, the purpose of this paper is to linearize T-S fuzzy model and makes direct use of linear control theories possible. To the best of our knowledge, there is no linearization technique applicable for T-S fuzzy model. The conventional linearization methods can not be used for T-S fuzzy model because fuzzy rules and membership functions are included in the T-S fuzzy model. So, this paper proposes new linearization technique for T-S fuzzy model by using T-S fuzzy state transformation. A T-S fuzzy model is transformed into linearizable form and then fuzzy feedback changes it into a linear controllable canonical form.

The linearizable condition of the proposed linearization technique is just controllability of linear local models which is easy to be checked and guaranteed. In the conventional linearization techniques, checking the size of the class of linearizable systems is considered as an open problem [9]-[11]. Therefore, The result of this paper can be considered as a new approximate linearization which has easier linearizable conditions for nonlinear systems. In this paper, the T-S fuzzy system with uncertainties is also considered. The SMC and optimal control are applied for the linearized T-S fuzzy system.

The important property of the sliding mode control is that the dynamics of overall system are determined by the sliding surface. The SMC input push the state onto the sliding surface and states can have the desirable dynamics of the surface in spite of uncertainties. Therefore, the system can be robust to parameter uncertainties and disturbances [12]-[15]. In this paper, a robust optimal controller is designed for T-S fuzzy model by using the proposed linearization and SMC.

The rest of this paper is organized as follows. In Section 2, T-S fuzzy system and controllers are presented and problem is formulated. In Section 3, the proposed linearization method is presented. In Section 4, robust optimal controller is designed for uncertain T-S model based on the proposed linearization and SMC. In section 5, numerical examples are given to illustrate the

achievement of the proposed linearization. In Section 6, a conclusion is drawn.

II. PROBLEM FORMULATION

The T-S fuzzy model been proposed by Takagi and Sugeno [1] to represent the local linear dynamic relations of nonlinear systems. The local linear model is described by fuzzy If-Then rules and will be employed to deal with the control design problem of nonlinear systems. The i th rule of the fuzzy model is of the following form:

Plant Rule i :

If $w_1(t)$ is F_{1l} and \dots and $w_g(t)$ is F_{gl}

$$\text{Then } \dot{x}(t) = A_i x(t) + B_i u(t) \quad (1)$$

for $i = 1, 2, \dots, L$

where F_{ig} is the fuzzy set, $A_i \in R^{n \times n}$, $B_i \in R^{n \times m}$, L is the number of If-Then rules, and $w_1(t), w_2(t), \dots, w_g(t)$ are premise variables.

By using a standard fuzzy inference method, that is, using a singleton fuzzifier, product fuzzy inference, and center-average defuzzifier, the T-S fuzzy model in (1) can be rewritten as

$$\begin{aligned} \dot{x}(t) &= \frac{\sum_{i=1}^L \mu_i(w(t)) \{A_i x(t) + B_i u(t)\}}{\sum_{i=1}^L \mu_i(w(t))} \\ &= \sum_{i=1}^L h_i(w(t)) \{A_i x(t) + B_i u(t)\} \end{aligned} \quad (2)$$

where $w(t) = [w_1(t), w_2(t), \dots, w_g(t)]$, $F_{ij}(w(t))$ is the grade of membership of $w_j(t)$ in F_{ij} and

$$\mu_i(w(t)) = \prod_{j=1}^g F_{ij}(w_j(t)).$$

In this paper, it is assumed that $\mu_i(w(t)) \geq 0$. For $i = 1, 2, \dots, L$ and $\sum_{i=1}^L \mu_i(w(t)) > 0$ for all t . Therefore, we get $h_i(w(t)) \geq 0$ for $i = 1, 2, \dots, L$ and

$$\sum_{i=1}^L h_i(w(t)) = 1. \quad (3)$$

Classical T-S controller has the following form

$$u(t) = \sum_{j=1}^L h_j(w(t)) u_j(t) \quad (4)$$

Overall T-S fuzzy system is written as follows.

$$\dot{x}(t) = \sum_{i=1}^L h_i(w(t)) \{A_i x(t) + B_i \sum_{j=1}^L h_j(w(t)) u_j(t)\} \quad (5)$$

Each local linear controller must be designed based on the stability conditions of the above system. Typical stability conditions are found in [1]-[3]. And the conditions are more conservative in the case of the system with uncertainties and time delays[7][8]. This makes it difficult to use linear control theories for T-S fuzzy system.

The best way of using linear control theories freely in the control of the T-S fuzzy system is linearization of them. Therefore, the problem of this paper is formulated as linearization of T-S fuzzy system into the following controllable form.

$$\dot{z}(t) = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & & \ddots & & \vdots \\ 0 & 0 & 0 & \dots & 1 \\ 0 & 0 & 0 & \dots & 0 \end{bmatrix} z(t) + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u(t) \quad (6)$$

III. PROPOSED T-S FUZZY FEEDBACK LINEARIZATION

In this section, a new linearization technique is proposed for T-S fuzzy model under the following assumption:

Assumption 1. All of the linear models are controllable. i.e., the following condition is satisfied:

$$\text{rank} \begin{bmatrix} B_i & A_i B_i & \dots & A_i^{n-1} B_i \end{bmatrix} = n \quad (7)$$

This is a very common condition for most control systems.

Under the above assumption, the following i -th rules of the fuzzy model are proposed to deal with the coordinate change for linearization.

Plant rule i :

If $w_1(t)$ is F_{1l} and \dots and $w_g(t)$ is F_{gl}

$$\text{Then } \dot{x}(t) = A_i x(t) + B_i u(t),$$

$$z(t) = T_i x(t) \quad (8)$$

$$\text{and } \dot{z}(t) = A_{ci} z(t) + B_{ci} u(t) \quad (9)$$

for $i = 1, 2, \dots, L$

where $A_{ci} = T_i A_i T_i^{-1}$, $B_{ci} = T_i B_i$.

After coordinate change, the overall fuzzy system is inferred from (9) as follows:

$$\dot{z}(t) = \sum_{i=1}^L h_i(w(t)) \{A_{ci} z(t) + B_{ci} u(t)\} \quad (10)$$

By using product fuzzy inference and center-average defuzzifier, the overall $z(t)$ can be rewritten as

$$z(t) = \sum_{i=1}^L h_i(w(t)) T_i x(t) \quad (11)$$

which is considered as the summation of the states $x(t)$ through transformation T_i with the proportion of h_i .

The above system can be a linearizable form by determining T_i as follows.

Under the assumption 1, the following T_i is obtained as follows:

$$T_i = \begin{bmatrix} B_{ci} & A_{ci}B_{ci} & \dots & A_{ci}^{n-1}B_{ci} \end{bmatrix} \begin{bmatrix} B_i & A_iB_i & \dots & A_i^{n-1}B_i \end{bmatrix}^{-1} \quad (12)$$

where the parameters in A_{ci} are obtained from the following characteristic equation of the i -th local linear model:

$$|sI - A_i| = s^n - a_{in}s^{n-1} - \dots - a_{i2}s - a_{i1} = 0 \quad (13)$$

Then the above state transformation T_i changes the i -th linear system into the following controllable canonical form:

$$\dot{z}(t) = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & & \ddots & & \\ 0 & 0 & 0 & \dots & 1 \\ a_{i1} & a_{i2} & a_{i3} & \dots & a_{in} \end{bmatrix} z(t) + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u(t) \quad (14)$$

The overall fuzzy system with local linear models (14) is now linearizable T-S fuzzy system.

$$\begin{aligned} \dot{z}(t) &= \sum_{i=1}^L h_i(w(t)) \{A_{ci}z(t) + B_{ci}u(t)\} \\ &= \begin{bmatrix} \sum_{i=1}^r h_i z_2 \\ \sum_{i=1}^r h_i z_3 \\ \vdots \\ \sum_{i=1}^r h_i a_i z(t) \end{bmatrix} + \begin{bmatrix} 0 \\ \vdots \\ 0 \\ \sum_{i=1}^r h_i \end{bmatrix} u(t) = \begin{bmatrix} z_2 \\ z_3 \\ \vdots \\ \sum_{i=1}^r h_i a_i z(t) \end{bmatrix} + \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u(t) \end{aligned} \quad (15)$$

where $a_i = [a_{i1} \ a_{i2} \ \dots \ a_{in}]$ and remind that

$$\sum_{i=1}^L h_i(w(t)) = 1 \text{ from (3).}$$

The following theorem presents a controller which linearizes T-S fuzzy system.

Theorem 1. The following nonlinear feedback input linearizes the T-S fuzzy system into the controllable canonical form (6):

$$u(t) = -\sum_{i=1}^L h_i(w(t)) a_i z(t) + v(t) \quad (16)$$

where the overall state $z(t)$ is inferred in (1). The proof is obvious from (15).

The Fig. 1 shows the overall description for the proposed linearization method.

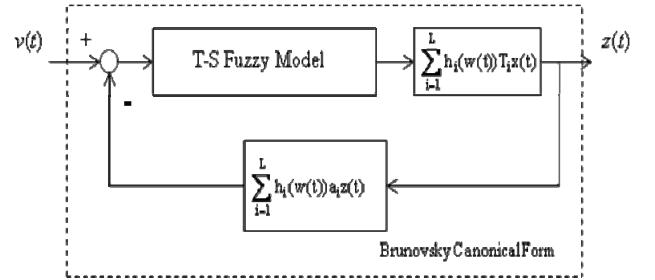


Fig.1. Overall scheme of T-S fuzzy feedback linearization

IV. ROBUST OPTIMAL CONTROL WITH SMC AND LINEARIZATION

In this section, the robustness of SMC is added to the linearized T-S fuzzy system. Consider T-S fuzzy system with uncertainties.

$$\dot{x}(t) = \sum_{i=1}^L h_i(w(t)) \{A_i x(t) + B_i u(t)\} + h(t) \quad (17)$$

where $h(t)$ is lumped uncertainties including parameter uncertainties and disturbances and bounded by

$$\|w(t)\| \prec w_{\max} \quad (18)$$

satisfying the following matching condition.

$$w(t) = B_i w_i(t) \text{ for } i = 1, \dots, L \quad (19)$$

In order to design robust optimal controller with SMC, the sliding surface which has the dynamics of optimal controlled system must be used. Such a sliding surface is designed as follows.

First, the virtual state is defined based on the following controllable canonical form of the nominal system :

$$\begin{bmatrix} \dot{z}_{o1}(t) \\ \dot{z}_{o2}(t) \\ \vdots \\ \dot{z}_{on-1}(t) \\ \dot{z}_{on}(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & 1 \\ 0 & 0 & 0 & \dots & 0 \end{bmatrix} \begin{bmatrix} z_{o1}(t) \\ z_{o2}(t) \\ \vdots \\ z_{on-1} \\ z_{on} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} v_o(t) \quad (20)$$

In this paper, the control objective of $v_o(t)$ is to minimize the following cost function.

$$J = \int_0^\infty \frac{1}{2} (z_0^T Q z_0 + r v_o^2) dt \quad (21)$$

The optimal input $v_o(t)$ is determined as the following form :

$$v_o(t) = -\frac{1}{r} B^T S z_o(t) = -K z_o(t) \quad (22)$$

where $K = [k_1 \ k_2 \ \dots \ k_n]$ and S is the solution of the following Riccati equation.

$$-SA - A^T S - Q + \frac{1}{r} SB^T BS = 0 \quad (23)$$

The virtual state is defined as follows:

$$\dot{z}_v(t) = -k_1 z_1(t) - k_2 z_2(t) - \dots - k_n z_n(t) \quad (24)$$

Sliding surface is defined as

$$\begin{aligned} S(z, z_v) &= z_v(t) + Kz(t) \\ &= z_v(t) + k_1 z_1(t) + k_2 z_2(t) + \dots + k_n z_n(t) \end{aligned} \quad (25)$$

If the state of the system (17) is on the sliding surface (25), the state has the dynamic of the nominal system (20) [14]. To guarantee the state on the sliding surface, the following hitting condition must be satisfied:

$$S(x)\dot{S}(x) < 0 \quad (26)$$

The above condition is satisfied by the discontinuous control input presented in Theorem 2.

Theorem 2. The SMC system with the following control input has the dynamics of the nominal optimal control system.

$$v(t) = (KB)^{-1} (k_n z_v(t) - KBw(t)_{\max} \cdot \text{sgn}(s)) \quad (27)$$

(Proof) See the proof of theorem2 in [14].

As mentioned in theorem 2 and sliding mode control theory, the state $x(t)$ follows the trajectory of the nominal system controlled by sliding mode control input $v(t)$ which is designed to put the states of the system onto the sliding surface.

The following initial virtual state makes the initial value of $s(z, z_v)$ equal to zero without reaching phase.

$$z_v(t_0) = -k_1 z_1(t_0) - k_2 z_2(t_0) - \dots - k_n z_n(t_0) \quad (28)$$

V. NUMERICAL EXAMPLE AND SIMULATION RESULTS

To show the robustness of the proposed robust optimal controller and its performance, consider an

example of a dc motor controlling an inverted pendulum via a gear train [4].

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \end{bmatrix} = \begin{bmatrix} x_2(t) \\ 9.8 \sin x_1(t) + x_3(t) \\ -10x_2(t) - 10x_3(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} u(t) + \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} h(t) \quad (29)$$

where $w(t)$ is a pulse train with the size of 0.5.

The above system can be described as follows:

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ \frac{9.8 \sin x_1(t)}{x_1(t)} & 0 & 1 \\ 0 & -10 & -10 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} u(t) + \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} h(t) \quad (30)$$

The local linear models in the T-S fuzzy model are as follows:

$$A_1 = \begin{bmatrix} 0 & 1 & 0 \\ 9.8 & 0 & 1 \\ 0 & -10 & -10 \end{bmatrix}, A_2 = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -10 & -10 \end{bmatrix}, B_1 = B_2 = \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} \quad (31)$$

The angle of the pendulum is $x_1(t)$, $x_2(t) = \dot{x}_1(t)$, and $x_3(t)$ is current of the motor. The $h_1(t)$ and $h_2(t)$ are fuzzy sets defined as

$$h_1(x_1(t)) = \begin{cases} \frac{\sin(x_1(t))}{x_1}, & x_1(t) \neq 0 \\ 1, & x_1(t) = 0 \end{cases}, \quad h_2(x_1(t)) = 1 - h_1(x_1(t)). \quad (32)$$

The membership functions are shown in Fig. 2.

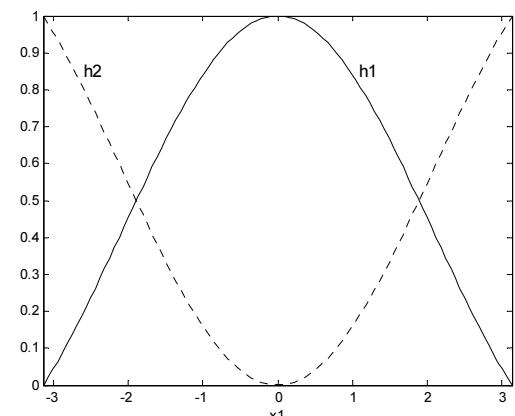


Fig. 2. Membership function

This fuzzy model exactly represents the dynamics of the nonlinear mechanical system under $-\pi \leq x_1(t) \leq \pi$.

The state transformation matrices is obtained as

$$T_1 = \begin{bmatrix} 0.1 & 0 & 0 \\ 0 & 0.1 & 0 \\ 0.98 & 0 & 0.1 \end{bmatrix} \text{ and } T_2 = \begin{bmatrix} 0.1 & 0 & 0 \\ 0 & 0.1 & 0 \\ 0 & 0 & 0.1 \end{bmatrix} \quad (33)$$

The controllable canonical forms are

$$A_{c1} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 98 & -0.2 & -10 \end{bmatrix}, \quad A_{c2} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -10 & -10 \end{bmatrix} \text{ and} \\ B_1 = B_2 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad (34)$$

From the above, the following vectors are identified:

$$a_1 = [98 \ -0.2 \ -10] \text{ and } a_2 = [0 \ -10 \ -10] \quad (35)$$

The following optimal controller for the linearized system is used.

$$v_o = -[3.1623 \ 4.6054 \ 3.1954]z_o \quad (36)$$

The virtual state is defined as follows.

$$\dot{x}_v = -3.1623z_2 - 4.6054z_3 - 3.1954z_v \quad (37)$$

Sliding surface is given by

$$s(z, z_v) = z_v + z_1 + 2z_2 + 3z_3 \quad (38)$$

By differentiating (38), the following is obtained.

$$\dot{s}(z, z_v) = -k_3z_v + k_3v + k_3h \quad (39)$$

The following novel sliding mode control input is obtained from the hitting condition.

$$v = \frac{1}{k_3} [k_3z_v - k_3h_{\max} \cdot \text{sgn}(s)] \quad (40)$$

Therefore the following initial virtual state can be obtained.

$$z_v(t_0) = -z_1(t_0) - 2z_2(t_0) - 3z_3(t_0) \quad (41)$$

As perfect linearization of the nonlinear system results in the Brunovsky canonical form, to verify the validity of the linearization, the responses of the system linearized by the proposed method is compared to the case of the Brunovsky canonical system.

The simulation results are shown in figures from Fig. 3 to Fig. 7.

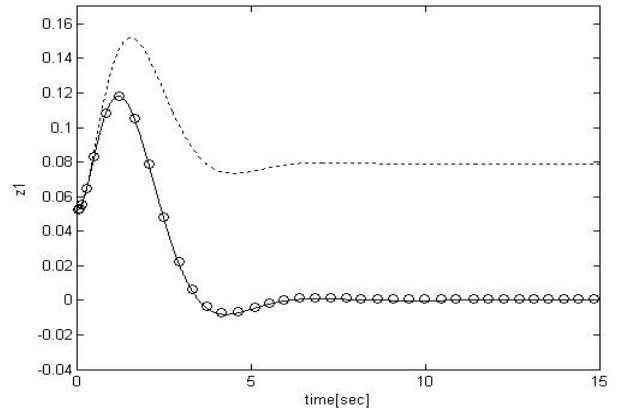


Fig. 3. State trajectories of z_1 .
— optimal control without uncertainty
---- optimal control with uncertainty
○ proposed control with uncertainty

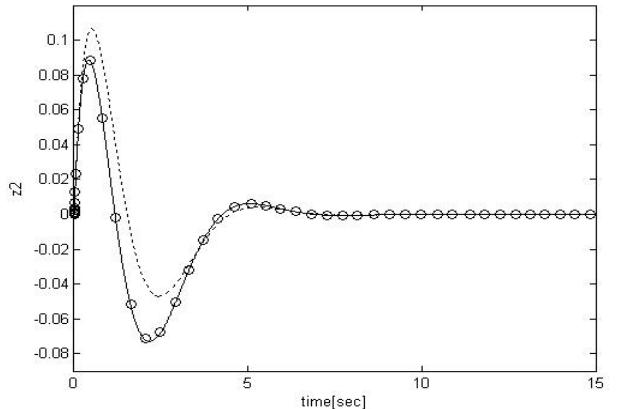


Fig. 4. State trajectories of z_2 .
— optimal control without uncertainty
---- optimal control with uncertainty
○ proposed control with uncertainty

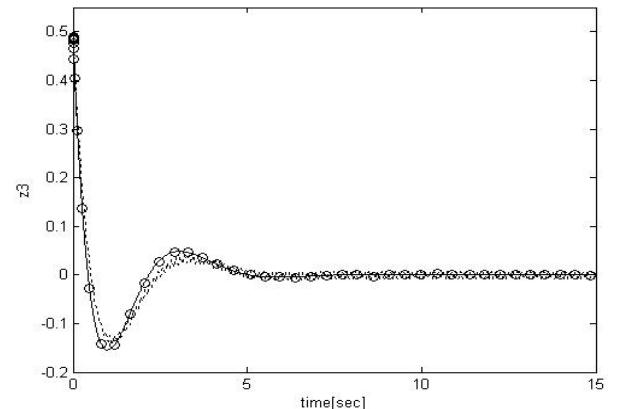


Fig. 5. State trajectories of z_3 .
— optimal control without uncertainty
---- optimal control with uncertainty
○ proposed control with uncertainty

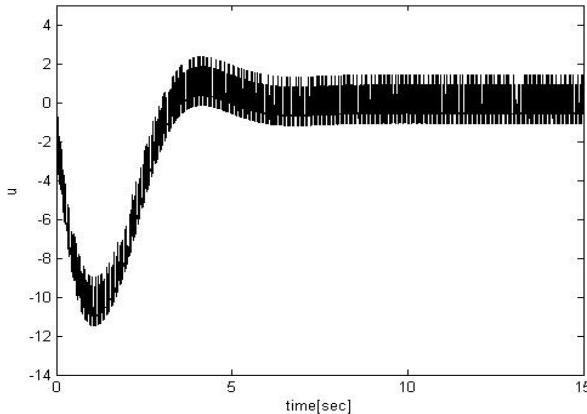


Fig. 6. Control input

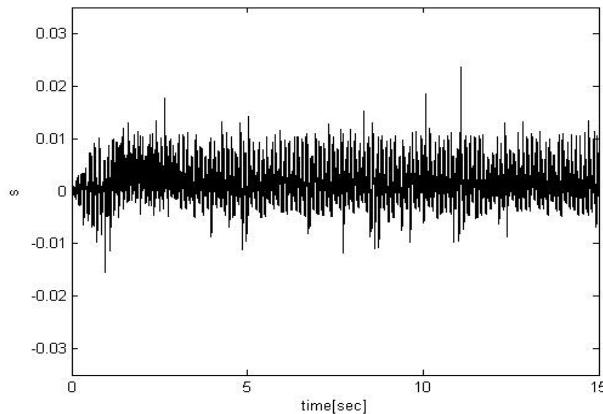


Fig. 5. Sliding function

For the T-S fuzzy system with uncertainty, the results of SMC optimal control based on the proposed linearization and the optimal control results for the uncertain T-S fuzzy system are compared to the response of the optimal control for the ideal Brunovsky canonical system with optimal controller. The proposed control case is almost same with the case of the optimal control with ideal Brunovsky canonical system. This means that the T-S fuzzy model has been linearized with sufficient exactness and the proposed robust optimal controller is robust and gives optimal performance. However, the optimal control reveals its weakness for uncertainties.

VI. CONCLUSIONS

Novel linearization of T-S fuzzy model is proposed by using the T-S fuzzy state transformation and fuzzy feedback and consequently, linear control theories can be used easily for T-S fuzzy systems. For the linearized system, robust optimal controller with SMC is designed and gives good performance in the presence of uncertainties. The linearization of T-S

fuzzy model can be considered as a approximate linearization of a nonlinear system approximated by T-S fuzzy system.

ACKNOWLEDGMENT

The authors of this paper were supported by the Second Stage of Brain Korea 21 Projects and Changwon National University in 2009-2010

REFERENCES

- [1] T. Takagi and M. Sugeno, "Fuzzy identification of systems and its applications to modeling and control," *IEEE transactions on systems, man, and cybernetics*, Vol. 15, pp.116-132,1985.
- [2] K. Tanaka, T. Ikeda, and H. O. Wang, "Fuzzy regulators and fuzzy observers: relaxed stability conditions and LMI-based designs," *IEEE Transactions on Fuzzy Systems*, Vol. 6,pp.250-265, 1998.
- [3] Bor-Sen Chen Chung-Shi Tseng, and Huey-Jian Uang, "Robustness Design of Nonlinear Dynamic Systems via Fuzzy Linear Control," *IEEE Transactions on Fuzzy Systems*,Vol.7, No.5, pp. 571-585, 1999.
- [4] K. Tanaka and H. O. Wang, *Fuzzy Control Systems Design and Analysis: A Linear Matrix Inequality Approach*, John Wiley & Sons, Inc., 2001.
- [5] Gang Feng, "A Survey on Analysis and Design of Model-Based Fuzzy Control Systems," *IEEE Transactions on Fuzzy Systems*, Vol.14, No.5, 2006.
- [6] Mohammad Narimani and H. K. Lam, "Relaxed LMI-Based Stability Conditions for Takagi–Sugeno Fuzzy Control Systems Using Regional-Membership-Function-Shape-Dependent Analysis Approach," *IEEE Transactions on Fuzzy Systems*, Vol.17, No.5, pp. 1221-1228, 2009.
- [7] Yan Zhao, Huijun Gao, J. Lam, Baozhu Du, "Stability and Stabilization of Delayed T-S Fuzzy Systems: A Delay Partitioning Approach," *IEEE Transactions on Fuzzy Systems*,Vol.17, No. 4, pp.750-762, 2009.
- [8] F.O. Souza, L.A. Mozelli, R.M. Palhares, "On Stability and Stabilization of T-S Fuzzy Time-Delayed Systems, *IEEE Transactions on Fuzzy Systems*, Vol. 17, No.6, pp.1450-1455, 2009.
- [9] H. G. Lee, Y. M. Kim, and H. T. Jeon, "On the linearization via a restricted class of dynamic feedback," *IEEE Transactions on Automatic Control*, vol.45, pp.1385–1391, 2000.
- [10] H. K. Khalil, *Nonlinear Systems*, Prentice Hall, 2002.
- [11] Hong-Gi Lee, Ari Arapostathis, and Steven I. Marcus, "Linearization of Discrete-Time Systems via Restricted Dynamic Feedback," *IEEE Transactions on Automatic Control*, Vol.48, No.9, pp.1646-1650, 2003.
- [12] K. D. Young, V. I. Utkin and U. Ozguner, "A control engineer's guide to sliding mode control," *IEEE Transactions on Control Systems Technology*, Vol7,No.3, pp.328–342, 1999.
- [13] Seung Kyu Park, Ho Kyun Ahn, "Nonconservative Sliding Mode Control with the Feedback Linearization or Nonlinear System," *Proceedings of the 39th IEEE Conference on Decision and Control* , pp.2210-2216, 2000.
- [14] S. K. Park, H. G. Ahn, " Robust optimal controller design with novel sliding surface," *IEE Proceedings Control Theory and Applications*, Vol.146, No.3, pp.242-246, 1999.
- [15] P. Liutanakul, S. Pierfederici, and F. Meibody-Tabar, "Application of SMC With I/O Feedback Linearization to the Control of the Cascade Controlled-Rectifier/Inverter-Motor Drive System With Small dc-Link Capacitor," *IEEE Transactions on Power Electronics*, Vol. 23, No.5,pp.2489 – 2499,Sept. 2008.



Min-Chan Kim Received the B. S., M. S., and Ph. D. degrees in Electrical Engineering from Changwon National University in 1996, 1998 and 2003, respectively. From 2006 to 2009, he was a research professor under the Brain Korea 21 Project Corps and is currently research professor under the Human resource development center for Offshore and Plant Engineering(HOPE) at Changwon National University. His research interests include in the area of H_∞ robust control theory, sliding mode control theory, system identification and its applications.



Ho-Kyun Ahn Received the B. S., M. S., and Ph. D. degrees in Electrical Engineering from Korea University in 1980, 1988 and 1992, respectively. He was a chief of Electrical Design Team, Hanshin Construction from 1980 to 1986. Since 1992, he is currently a professor in the Department of Electrical Engineering at Changwon National University, Changwon, Korea. His research interests include in the area of power electronics, power conversion and alternative energy.



Fa-Guang Wang Received the B.S and M.S degrees in Control Science and Engineering at Huazhong University in 2006 and Electrical Engineering at Changwon National University in 2008, respectively. Now is in Changwon National University for Ph. D degree. His research interests include in the area of adaptive control, fuzzy control, support vector machines and sliding mode control.



Seung-Kyu Park Received the B. S., M. S., and Ph. D. degrees in Electrical Engineering from Korea University in 1984, 1986 and 1990, respectively. He was a visiting professor of Strathclyde University, England from 1995 to 1996. Since 1990, he is currently a professor in the Department of Electrical Engineering at Changwon National University, Changwon, Korea. His research interests include in the area of adaptive control theory, robust control theory



Gun-Pyong Kwak Received the B. S., M. S., and Ph. D. degrees in Electrical Engineering from Korea University in 1982, 1985 and 1990, respectively. He was a section chief of CNC team, LGIS from 1990 to 1997. Since 1998, he is currently a professor in the Department of Electrical Engineering at Changwon National University, Changwon, Korea. His research interests include in the area of control algorithm and motion controller.



Tae-Sung Yoon Received the B. S., M. S., and ph. D. degrees, in Electrical Engineering from Yonsei University, Seoul, Korea, in 1978, 1980 and 1988, respectively. He worked with the Department of Electrical Engineering at the 2nd Naval Academy, Jinhae, Korea, as a member of the teaching staff from 1980 to 1983. He worked with the Department of Electrical Engineering at Vanderbilt University, Nashville, as a Visiting Assistant Professor from 1994 to 1995. Since 1989, he has been with the Department of Electrical Engineering, Changwon National University, Changwon, Korea where he is currently a Professor. His research interests include robust filtering and mobile robotics.