Investigation of Setting Process of Cementitious Materials Using Electromechanical Impedance of Embedded Piezoelectric Patch

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Abstract

In this study, the evolution of the electro-mechanical impedance (EMI) of a piezoelectric (PZT) patch embedded in fresh cement paste was investigated to discuss the possibility of monitoring the setting process of cement-based materials using an EMI sensing technique. A tailored thin square PZT patch was embedded in cement paste before casting, and EMI signatures of the embedded patch were continuously measured from casting up to 12 hours. A standard penetration resistance test was performed to compare and correlate the evolution of EMI during the setting process. The results showed that EMI responses differ according to the age of the cement paste, and that the behavior of the EMI resonance peak has a clear correlation with the penetration resistance of the cement paste. Based on the results, it is concluded that an EMI sensing technique using embedded PZT patch can be effectively applied to monitor the setting process of cement-based materials.

Keywords : cement hydration, electromechanical impedance, piezoelectric, setting process monitoring

1. Introduction

Cement-based material such as concrete is a multiphase material that endures significant phase changes at a micro-structural level along cement hydration. At the beginning of cement hydration it behaves like a liquid, and after a certain period of time, the transition period known as the setting process starts when cement-based material begins to solidify. Finally, at the end of the liquid to solid transition, it starts to continuously gain strength over time in the subsequent hardening

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period[1]. Information on when the process of solidification begins and ends is very important for quality control and work scheduling. It is therefore necessary to develop a test or a monitoring method that will provide information on the time required for the setting of cement-based materials.

On the other hand, recent advances in smart sensing technologies have added a new dimension on nondestructive monitoring of structural integrity and conditions of structures. Of the related technologies, the electro-mechanical impedance (EMI) sensing technique using piezoelectric patch has shown great potential for the implementation of a built-in online structural health monitoring system[2].

Very recently, the EMI sensing technique has been successfully applied for strength gain monitoring of concrete[3,4,5,6]. In EMI sensing setup for strength gain monitoring, a PZT patch is

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adhesively bonded on the surface of the host substrate (i.e. concrete) to couple the patch and the host[3,4,5,6]. However, surface bonding is not available for a liquid state concrete[6]. Therefore, although successful, the current EMI sensing technique for early-age concrete monitoring can only be applicable to solidified (i.e. hardened state) concrete, and cannot be applied to monitor the liquid state concrete that undergoes the setting process. Due to this limitation, EMI evolution of early age concrete - as early as immediately after mixing - is still unknown. The main purpose of this study is to investigate the evolution of the EMI response of a PZT patch embedded in hydrating cement paste, and thereby to discuss the possibility and effectiveness of the use of an embedded EMI sensing technique to monitor the hydrating setting process of cement-based materials.

2. Principle of EMI sensing technique

The basic principle of an EMI sensing technique is to monitor variations in the mechanical impedance of a host structure via the electrical impedance of a piezoelectric patch attached to the host medium. In EMI sensing, the piezoelectric patch (such as PZT patch) functions simultaneously as both a sensor and an actuator; to mechanically excite the structure and to measure the mechanical response (velocity) of the structure. Specifically, if a sinusoidal voltage is applied to a piezoelectric patch attached to a host structure. it causes the local area of the structure, where the patch is attached, to vibrate due to the direct effect of piezoelectricity. At the same time, this mechanical vibration response induces an electric current in attached patch the due to the converse piezoelectric effect. Therefore, if we measure the input electric voltage (mechanical force) and output electric current (mechanical vibration) of the piezoelectric patch, electrical (and hence mechanical) impedance, which is defined as the ratio of the voltage (force) applied to the resulting electric current (velocity), can be obtained. Liang et al.[7] proposed the following EMI model of a 1-D PZT-structure interaction system:

$$Y(\omega) = \frac{I(\omega)}{V(\omega)} = G(\omega) + jB(\omega)$$
$$= j\omega a \left(\overline{\epsilon_{33}^T} - \frac{Z_P(\omega)}{Z_S(\omega) + Z_P(\omega)} (d_{3x})^2 \overline{Y_{xx}^E} \right)$$

where $Y(\omega)$ is the electrical admittance (inverse of impedance) of a PZT patch attached to a host structure. $I(\omega)$ is the output current. $V(\omega)$ is the excitation voltage. $G(\omega)$ is the real of the admittance (conductance), $B(\omega)$ is the imaginary part of the admittance (susceptance). *j* is $\sqrt{-1}$. ω is the excitation frequency, a is the geometric constant of the transducer, $\overline{\epsilon}_{33}^T$ is the complex electric permittivity of the patch (at constant field). d_{3x} is the piezoelectric strain stress coefficient in the arbitrary x direction, and \overline{Y}_{xx}^{E} is the complex Young's modulus of the patch (at constant electric field). Finally, $Z_P(\omega)$ is the mechanical impedance of the patch and $Z_S(\omega)$ is that of the host structure. Assuming that mechanical impedance of the PZT patch does not change during the monitoring period, the admittance will be solely dependent on the mechanical impedance, $Z_S(\omega)$, of the host medium, therefore the subsequent changes and in admittance signature will be due to changes in the mechanical impedance of the host. Any changes in mechanical properties such as stiffness of the host medium will influence the mechanical impedance of the host structure.

3. Experimental setup

In this study, cement paste was used in order to eliminate the effect of additives such as aggregates and thus to investigate pure EMI evolution in hydrating cement-based materials. The cement paste was prepared by 90-second manual mixing of ordinary Type I Portland cement and tap water, with a water to cement ratio of 0.40. The chemical composition of the cement provided by manufacturer is listed in Table 1.

Table 1. Chemical Composition of Type 1 Portland Cement (% by weight)

Chemicals	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	SO3	K₂O	lg. Loss
Contents	21.54	5.15	3.58	61.63	3.08	2.10	1.32	1.40

To monitor the EMI response of freshly mixed liquid state cement paste, a PZT patch is embedded in the cement paste. A tailored square PZT patch (PZT5A Navy type II. Piezo Systems Inc.) $10 \times 10 \times 0.2mm$ in size was used. The PZT patch was placed at the approximate center of the metal cubic mold $(50 \times 50 \times 50 mm)$. The paste was cast in the mold immediately after mixing. One of the technical concerns regarding the embedded PZT patch is the risk of a short circuit due to the presence of water. To prevent a short circuit of the embedded PZT patch. non-conductive unsaturated polyester resin is thinly coated on the surface of the PZT patch before it is embedded. The experimental setup for EMI sensing using the embedded PZT patch is illustrated in Figure 1. A commercial LCR meter (HIOKI 3532-50 LCR HiTESTER) was used for the EMI measurements. All the measured data was recorded using a personal computer through a GP-IB interface connected to the LCR meter. Immediately after the casting, initial measurement of the EMI of the PZT

patch embedded in the cement paste was conducted. After the initial subsequent measurement. measurements were conducted every 10 minutes for the first 12 hours (total of 72 time steps) to investigate the setting process. At each measurement, the admittance (inverse of impedance) signature was measured five times repeatedly and averaged to remove incoherent noise. The frequency range from 50 kHz to 350 kHz (500 Hz interval) was chosen for measuring EMI signal, as this is a favorable range for early-age concrete property monitoring[3,4]. It is also noted that the real part of the admittance (conductance) is more preferable for monitoring the mechanical changes in the host medium due to the capacitive nature of the PZT patch[3,4,5]. So, only the conductance signature is considered in this study.

In addition to the EMI measurements, a penetration resistance test was conducted to compare with the EMI responses during the setting process. The penetration resistance test is a standard method (ASTM C 403) to determine the initial and final setting times of cement mortar[8]. Note that it also can be successfully applied to monitor the setting of the cement paste[9]. In the test, the load required for a needle to penetrate a cement paste sample to the depth of 25mm was measured, and the penetration resistance was calculated from the ratio of the required load to the cross-sectional area of the penetrating needle.



Figure 1. Configuration of EM conductance measurement of cement paste

4. Results and Discussions

4.1 Initial EMI Response

Figure 2 shows conductance (the real part of the admittance) of the PZT patch in the air (i.e., before it was embedded) and in the freshly mixed cement paste (immediately after casting). As seen in this figure, the conductance signatures for both cases are slightly different, but show clear peak behaviors. This confirms that a short circuit has been successfully prevented, and suggests that the EMI sensing can be possible even after a PZT patch is embedded in liquid. The difference between two cases is mainly due to the mechanical impedance change of the surrounding material of the PZT patch, i.e. the air and the liquid state cement paste. When a harmonic electric voltage is applied on a PZT patch, it vibrates freely.



Figure 2. Measured conductance of PZT patch before and after Embedment

However, vibration mode and magnitude of the patch are altered with mechanical impedance of surrounding medium[10]. Just after mixing, the cement paste is in a viscoelastic state[11]. For a PZT patch embedded in this viscoelastic cement paste, the viscosity of the paste and the hydrostatic fluid pressure can reduce the vibration magnitude of the PZT patch. However, in this case, the vibration mode of the patch would not be changed, since the mechanical impedance of the liquid is very low compared with that of the solid PZT patch. It is evident in Figure 2 that the frequency of the largest EM resonance peak of the patch is identical (172 kHz) for both cases, while the magnitude of the peak was slightly reduced, from 0.0391 to 0.0366.

4.2 Evolution of EMI during Solidification Process

Figure 3 shows the measured EM conductance signatures from initial 0 to 6 hours after casting. while Figure 4 shows those from 6 to 12 hours. It is seen that the conductance responses of the patch are different (but show a unique trend) with the age of cement paste. This suggests that EMI sensing using the embedded PZT patch can be applicable to monitor the hydration process of very early age cement-based materials. Significant changes in EMI resonance peaks are observed. The magnitude of the first largest EMI peak is gradually reduced, and the sharpness of the peak degrades with age. It is also seen that the frequency of the first peak remains constant (around 172 kHz) until 2 hours, and then gradually shifts toward a higher frequency region. The sharpness of the peak also rapidly degrades after 2 hours. The peak can hardly be identified visually after 8 hours, and no significant peaks are observed at 12 hours. Figure 5 shows the peak frequency values with respect to the ages of cement paste up to 8 hours after casting. Peak frequencies after 8 hours were not available, as they could not be identified visually in the EMI signatures. It is seen that the peak frequency value increases rapidly in an exponential manner after 3 hours.



Figure 3. Measured conductance of embedded PZT patch (from 0 to 6 hours after casting)



Figure 4. Measured conductance of embedded PZT patch (from 6 to 12 hours after casting)

Figure 6 shows the penetration resistance at every hour, from initial to 8 hours after casting. An exponential increase in penetration resistance is observed with respect to time, which is very similar with that of the EMI resonance peak frequency. The resistance until the age of 4 hours was less than 1MPa and at the age of 8 hours was as high as 37MPa. The exponential increase in penetration resistance is a typical behavior of a hydrating cement-based material such as mortar or cement paste[9]. One distinct feature in the penetration resistance from the EMI resonance peak frequency is that the rapid increment of the penetration resistance value is observed after 4 hours from casting, while that of the peak frequency is observed after 3 hours. Figure 7 shows the correlation between the EMI resonance peak frequency and the penetration resistance. A strong correlation (a second order polynomial fit with high correlation coefficient of 0.99) between them is observed. It should be noted that the 7 equation provided in Figure cannot be generalized. since the EMI resonance peak frequency may also be affected by other factors such as water/cement ratio. Factors affecting EMI resonance peak behavior during cement hydration are currently under investigation. Discussions on the results are provided as follows.



Figure 5. EMI resonance peak frequency as a function of material age



Figure 6. Penetration resistance as a function of material age

Immediately after mixing, the cement grains are dissolved in the water and then the reaction between the cement and water begins. The reaction between cement and water results in the formation of calcium hydroxide. a crystallized compound, and a colloidal gel constituted by hydrated compounds like C-S-H. which develops around the cement grains (and similarly around the PZT patch). As hydration progresses, the hydrates around the cement grains grow, first to form small isolated clusters and then bigger clusters. The isolated clusters are weakly connected to each other to form a network, and after a certain time. a solid percolation path is formed in the cement paste (solid percolation threshold)[12]. It is well known that the shear modulus of the cement paste starts to develop beyond the percolation threshold [11,13]. The magnitude of the EMI resonance peak decreases as the age of cement paste increases, as the development of a hydrated compound in the vicinity of the embedded PZT patch suppresses the vibration of the patch. However, the vibration mode of the patch would not be significantly changed until the clusters in the vicinity of the patch are connected to each other to develop shear modulus. This is why both the frequency of the EMI resonance peak and the penetration resistance did not change until 2 hours after casting. The liquid state cement paste cannot resist the shear force applied by the penetration needle. On the other hand, when the PZT patch is coupled with the network of solid clusters, the vibration mode of the PZT patch would be significantly changed as shear stiffness in the boundary of the patch starts to develop. Normally, the EMI resonance frequency of the PZT patch attached to the solid host medium shifts to the higher frequency region as the mechanical impedance of the host medium increases [3,4,5]. This supports the frequency shifting behavior of the embedded PZT patch after 3 hours and the increasing behavior of the penetration resistance value. It is worth noting that a significant increment of the penetration resistance value has been visibly identified after 4 hours in this study. Therefore, it can be inferred that, within this study, the initial setting (i.e. solid percolation threshold) took place 3 hours after casting based on the EMI results and 4 hours after casting based on the penetration resistance result.

The interconnected solid network continues to develop, even after the percolation threshold is reached, until it spreads throughout the material during the solidification process[11]. Therefore, the more the solid network develops, the more the vibration of the PZT patch is restrained so that the amplitude of EMI resonance peak decreases (and hence the value of the penetration resistance increases) as the solidification process proceeds. Normally, the final setting time is defined as the end of the solidification process and the beginning of the hardening process. However, since both the solidification and the hardening (strength development) processes are the result of the cement hydration, it is hard to distinguish one from another through a standard test method such as the penetration resistance test[9]. Therefore, in the standard test method, the final setting is empirically defined when the penetration resistance value reaches 12MPa for cement paste[8,9]. In this study, the final setting took place between 7 and 8 hours after casting based on the penetration resistance result shown in Figure 5. Similarly, the EMI resonance peak could hardly be identified visually after 8 hours from casting (see Figure 4). This confirms the effectiveness of the embedded PZT patch based EMI sensing technique as an approach to determining the final setting time of cement paste. Moreover, the magnitude of the EMI response decreased, even after 8 hours. This suggests that the subsequent hydration process of cement paste even after the final setting can be monitored by EMI sensing. Therefore, it can be concluded that the EMI sensing technique using embedded PZT patch can be effectively used not only to determine the initial and final setting times, but also to monitor the continual reaction of hydrating cement paste.



Figure 7. Correlation between penetration resistance and EMI resonance peak frequency

5. Conclusion

In this study, the evolution of the EMI of PZT patch embedded in cement paste during setting process is investigated. A tailored thin square PZT patch was embedded in cement paste before casting and EM admittance signatures were continuously measured from immediately after casting up to 12 hours. EMI responses showed a clear trend with respect to the ages of hydrating cement paste. In particular, the behavior of the EMI resonance peak during the setting process has a strong correlation with that of the penetration resistance value. The initial and final setting times determined by the penetration resistance test matched well with the times when critical changes in EMI resonance peak occurred. Initial setting time related with the shifting of EMI resonance peak while the final setting time related with the peak disappearance. Based on these results, it can be concluded that the property changes of very early age cement-based materials, as early as from casting, can be successfully and sensitively monitored through an EMI sensing technique using an embedded PZT patch.

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