Inflow Condensation Heat Transfer Characteristics of CO₂ in Microchannel

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Introduction

Carbon dioxide refrigeration system has been utilized for water heaters, mobile air conditioning systems, bending machines, and room air conditioners. Now, the system expands its applications to large capacity systems, such as supermarkets, industrial low temperature applications, and commercial refrigeration storage. The operation temperature of the CO2 refrigeration systems for the above applications is normally so low that the condensation process is accompanied with the heat rejection process. For example, CO₂/NH₃ cascade system is one of the promising options for commercial or industrial refrigeration systems. In this case, condensation of CO₂ occurs inside the cascade condenser. As operating conditions of the CO₂ system are widening, the condenser of the CO2 system is becoming an important component. Therefore, understanding of CO₂ condensation phenomena

with/without oil and development of a properly estimating model for CO₂ condensation heat transfer and pressure drop are required.

Park and Hrnjak¹⁾ tested the CO₂ condensation heat transfer and pressure drop with a microchannel having a hydraulic diameter of 0.89 mm. They suggested that the Thome et al. model²⁾ and the Mishma and Hibiki model³⁾ for estimating heat transfer coefficient and predicting pressure drop, respectively. In the previous studies, the researches on CO2 condensation process were very limited especially in terms of flow patterns, test tubes with microchannels, and effects of lubricants. Besides, the existing prediction models for heat transfer coefficient and pressure drop need to be verified for the CO₂ condensation, and if necessary they should be developed. The objective of the present study is to investigate the flow patterns in narrow channel and the effects of oil on condensation heat transfer coefficient and pressure drop of CO₂ under relatively low temperature conditions. We developed the new models for estimating the CO₂ condensation heat transfer coefficient in smooth tube, microchannels, and microfin tubes, and suggested the previous models for estimating CO₂ condensation pressure drop.

Experiments

Figure 1 shows a schematic of the experimental setup. The test setup was composed of a magnetic gear pump, preheater, test section, subcooler, chillers, constant temperature bath, and receiver tank for safety. The working fluid was pure CO₂, and the secondary fluid for the preheater and the test section was an Ethylene Glycol (EG) and water mixture (brine), with a concentration of 40% of EG. The CO₂ condensation heat transfer coefficient (hi) was calculated by Eq. (1). The thermal resistance of the microchannel wall was neglected in Eq. (1), which was estimated by less than 0,2% compared to that of

fluids. The UA value in Eq. (1) was obtained by using the heat transfer amount from CO₂ to brine, and temperatures of inlets and outlets of CO₂ and brine as shown in Eq. (2). The brine-side heat transfer coefficient was determined by utilizing the Wilson Plot method as shown in Eq. (3).

$$\frac{1}{UA} \frac{1}{h_0 A_0} + \frac{1}{h_i A_i} \tag{1}$$

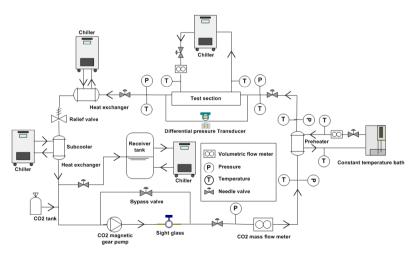
$$Q = UA\Delta T_{lm} \tag{2}$$

$$N_0 = 0.0971 \times (\text{Re}^{0.5} \text{Pr}^{0.3})$$
 (3)

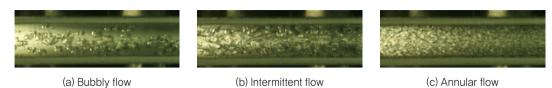
Results and discussion

Flow visualization

Figure 2 shows the representative images of flow patterns of CO₂ condensation in the narrow channel. The present flow patterns were classified by the following definitions. Bubbly flow: Small bubbles separately flow along channel. Intermittent flow: Large bubbles from merging small bubbles flow at the center of channel,



[Figure 1] Schematics of experimental setup

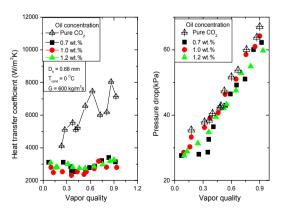


[Figure 2] Flow patterns of CO₂ condensation in narrow channel

and liquid-phase CO₂ flows close to wall. The boundaries between bubbles can be found, and boundaries between liquid-phase and bubbles are wavy and irregular. Annular flow: Thin liquid film is formed at the wall and the shape of liquid film is very steady. Most part of channel is occupied by vapor-phase CO₂

Effects of oil on heat transfer coefficient and pressure drop

Figure 3 shows the effects of oil concentration on CO₂ condensation heat transfer coefficient and pressure drop. The heat transfer coefficient significantly decreased with oil concentration. Decrease of condensation heat transfer coefficient with oil addition came from the increased thermal resistance by oil-film at tube wall, which prevents the vapor CO₂ from directly



[Figure 3] Effects of oil on CO₂ condensation heat transfer coefficient and pressure drop

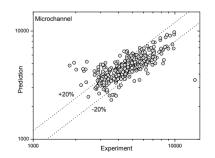
contacting on tube wall.

Developing new models for condensation heat transfer coefficient of CO₂

We developed a new model for the condensation heat transfer coefficient of CO₂ by allowing for the liquid film thickness and smooth interface shape of the liquid film. Eq. (4) shows the present model, and **Table 1** shows constants in Eq. (4). The non-dimensional form of liquid film thickness, the ratio of the Weber number and the Froude number were utilized to

(Table 1) Constants in the present model

Constants	Smooth tube	Microchannel
а	226.04	19.72
b	0.25	0.43
С	0.75	0.3
d	-0.39	-0.31
е	-0.3	-0.39
f	-0.21	-0.59



[Figure 4] Deviations between experiment and prediction for microchannels

consider the thick liquid film and the interface shape between liquid and vapor for CO₂ condensation. The mean deviations between the present model and the experimental results were 28.9%, and 18.9% for smooth tube and microchannels, respectively. **Figure 4** showed deviations between experiment and prediction for microchannels. Among the total data number of 346, data of 76% were within and 86% of data were within.

$$h = \alpha \times \operatorname{Re}_{l}^{b} \times \operatorname{Pr}_{l}^{c} \times \left(\frac{We}{Fr}\right)^{d} \left(\frac{\delta}{D}\right)^{e} P_{r}^{f} \tag{4}$$

Conclusions

In this study, two-phase flow patterns of CO₂ condensation in narrow channel and effects of oil concentration on the heat transfer coefficient and pressure drop of CO₂ condensation in microchannel were investigated. Besides, a prediction model of CO₂ condensation heat transfer coefficient in smooth tube and microchannels were developed.

(1) The present flow patterns were categorized by bubbly, intermittent, and annular flow. The transition vapor quality from intermittent flow to annular flow became advanced with an increase of mass flux and with a decrease of condensation temperature.

- (2) When oil concentration was changed from 0.7 to 1.2 wt. % the heat transfer coefficient decreased by about 50% as compared to that of the pure CO₂. In contrast, the pressure drop slightly decreased as compared to that of pure CO₂.
- (3) A model for the condensation heat transfer coefficient of CO₂ was developed by considering the film thickness and the interface shape of the liquid film. The mean deviations between the present model and the experimental results were 28.9% and 18.9% for smooth tube and microchannels, respectively.

References

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